
APPENDIX I-1.
PRELIMINARY HYDROLOGY STUDY

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PRELIMINARY HYDROLOGY STUDY
FOR
PIRAEUS POINT
PIRAEUS STREET, ENCINITAS, CA 92024
MULTI-005158-2022

CITY OF ENCINITAS, CA

PREPARED FOR:

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A handwritten signature in black ink, appearing to read "Ty G. Lawson", written over a horizontal line.

TYLER G. LAWSON, RCE 80356

DATE

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1.0 EXECUTIVE SUMMARY

1.1 Introduction

This Preliminary Hydrology Study for the proposed development at the intersection of Piraeus Street and Plato Place has been prepared to analyze the hydrologic and hydraulic characteristics of the existing and proposed project site. This report intends to present both the methodology and the calculations used for determining the runoff from the project site in both the existing condition and the post-developed (proposed) condition produced by the 100-year, 6-hour storm.

1.2 Existing Conditions

The subject property is located east of Interstate 5 and is geographically settled between Piraeus Street to the east and Plato Place to the south. The site is bordered by single family homes to the east, Interstate 5 to the west, and undeveloped open space to the north and south. The site is currently vacant and has not previously been developed. Existing site topography is generally steep with slopes ranging from 4 to over 75 percent and elevations ranging from 175 to 69 feet.

The existing site is comprised of approximately 8.16 acres. In its current state, about 70% of the site drains north via surface/sheet flow before entering an existing storm drain conveyance system at the northwest corner of the property. This is shown as drainage areas B-1 and B-2 on the Existing Condition Hydrology Node Map included in Appendix A. Once in the storm drain system, runoff from Drainage area B-1 and B-2 flows west, crossing Interstate-5 into an earthen ditch. The remainder of the site, areas A-1 and A-2, as shown on the Existing Condition Hydrology Node Map in Appendix A, flow south via surface/sheet flow and enters the existing storm drain system at the southwest corner of the property. The existing system carries runoff across Interstate-5 and discharges into an existing concrete lined ditch where it will meet runoff from Drainage Area B-1 and B-2. From this point, drainage from both basins continues north until the runoff reaches Batiquitos Lagoon and finally the Pacific Ocean.

An existing condition and post-development hydrology analysis of the existing system has been included as a part of this study to ensure the proposed project will not negatively impact the existing storm drain system. Results of the offsite analysis are provided in the Conclusions section of this report. Supporting calculations and AES output reports are provided in Appendix C.

In the existing condition, pavement, and various hardscape results in a 0% impervious basin. Based City of Encinitas Engineering Design Manual, the basin was analyzed assuming Type D soils. Based upon soil type and the lack of existing impervious area onsite, a runoff coefficient of 0.45 was used for each basin. Using the Rational Method Procedure outlined in the San Diego County Hydrology Manual, a peak flow rate and time of concentration was calculated for the basin for the 100-year, 6-hour storm event. Refer to the existing condition hydrology calculations included in Appendix C of this report for detailed analysis and the

Existing Condition Hydrology Node Map included in Appendix A of this report for existing drainage basin delineation and POC'S.

1.3 Proposed Project

As shown on the Post-Development Hydrology Node Map, runoff from Drainage Area's A-1 thru A-18 is picked up in the on-site storm drain system and conveyed to the south to the proposed biofiltration basin located adjacent to Plato Place. Once the runoff is treated and stored it is discharged into the existing storm drain system identified as POC-A.

Runoff generated in Drainage Areas B-1 thru B-6 primarily sheet flows west towards Piraeus Street where it is collected in a concrete ditch and discharges into an existing headwall at the northwest corner of the site. This is identified as POC-B on the Post-Construction Node Map.

A Runoff coefficient was calculated for Drainage Basin- A based on the methodology described in the City of Encinitas Engineering Design Manual and the formula provided therein. See Section 2.4 of this report for post-development runoff coefficient calculations. For a breakdown of the existing condition and post development peak flow rates for the 100-year, 6-hour storm event, see the conclusion section of this report.

In an effort to comply with the City of Encinitas' Stormwater standards and the MS4 Permit, all runoff generated onsite will be conveyed to a biofiltration basin adjacent to Plato Place as shown on the Post Development Hydrology Node Map. The biofiltration basin has been sized for pollution and flow control purposes. Flow rates generated on-site will be controlled via a small low-flow orifice consistent with HMP requirements as outlined in the City of Encinitas BMP Manual. In larger storm events, runoff not filtered through the engineered soil will be conveyed via an overflow outlet structure consisting of a 3-foot by 3-foot grate located on top of the outlet structure. Runoff conveyed via the outlet structure will bypass the treatment and flow control BMP's and will be conveyed directly to the proposed storm drain system perpendicular to Piraeus Street.

Conclusions

Onsite

As illustrated in the Peak Flow Rate Comparison Table shown below, the project has been designed to adequately convey the 100-year, 6-hour storm event. In addition, in the mitigated post development condition, the site has been designed to attenuate the 100-year storm event and reduce flow rates below what is currently leaving the site today. Based on our analysis, the proposed storm drain system has sufficient capacity to convey the flows that are generated by this development.

Peak Flow Rate Comparison Table (100 Year, 6 Hour)			
Existing Condition		Post Development (Unmitigated)	
Drainage Area	Peak Flow (CFS)	Drainage Area	Peak Flow (CFS)
A-1 THRU A-2	4.90	A-1 THRU A-18	29.89
B-1 THRU B-2	10.17	B-1 THRU B-9	4.90

Peak Flow Rate Comparison Table (100 Year, 6 Hour)			
Existing Condition		Post Development (Mitigated)	
Drainage Area	Peak Flow (CFS)	Drainage Area	Peak Flow (CFS)
A-1 THRU A-2	4.90	A-1 THRU A-18	0.12
B-1 THRU B-2	10.17	B-1 THRU B-9	4.83

1.4 References

“Encinitas Stormwater Manual Chapter 7”, Version 1.3, adopted March 17, 2010, City of Encinitas, Engineering Department

“Engineering Design Manual Chapter 6: Drainage Design Requirements”, revised February 2016, City of Encinitas

“Engineering Design Manual Appendix 6: Drainage Design Requirements”, October 28, 2009, City of Encinitas

“Engineering Design Manual Chapter 7: BMP Design Manual”, revised February 2016, City of Encinitas

Soil Survey Staff, Natural Resources Conservation Service, United States Department of Agriculture. Web Soil Survey. Available online at <http://websoilsurvey.nrcs.usda.gov>. Accessed May 2015

2.0 METHODOLOGY

2.1 Introduction

The hydrologic model used to perform the hydrologic analysis presented in this report utilizes the Rational Method (RM) equation, $Q = CIA$. The RM formula estimates the peak rate of runoff based on the variables of area, runoff coefficient, and rainfall intensity. The rainfall intensity (I) is equal to:

$$I = 7.44 \times P_6 \times D^{-0.645}$$

Where:

I = Intensity (in/hr)
 P_6 = 6-hour precipitation (inches)
 D = duration (minutes – use T_c)

Using the Time of Concentration (T_c), which is the time required for a given element of water that originates at the most remote point of the basin being analyzed to reach the point at which the runoff from the basin is being analyzed. The RM equation determines the storm water runoff rate (Q) for a given basin in terms of flow (typically in cubic feet per second (cfs) but sometimes as gallons per minute (gpm)). The RM equation is as follows:

$$Q = CIA$$

Where:

Q = flow (in cfs)
 C = runoff coefficient, ratio of rainfall that produces storm water runoff (runoff vs. infiltration/evaporation/absorption/etc)
 I = average rainfall intensity for a duration equal to the T_c for the area, in inches per hour.
 A = drainage area contributing to the basin in acres.

The RM equation assumes that the storm event being analyzed delivers precipitation to the entire basin uniformly, and therefore the peak discharge rate will occur when a raindrop that falls at the most remote portion of the basin arrives at the point of analysis. The RM also assumes that the fraction of rainfall that becomes runoff or the runoff coefficient C is not affected by the storm intensity, I, or the precipitation zone number.

Rational Method calculations were performed using the AES-2016 computer program. To perform the hydrology routing, the total watershed area is divided into sub-areas which discharge at designated nodes. The procedure for the sub-area summation model is as follows:

1. Subdivide the watershed into an initial sub-area (generally 1 lot) and subsequent sub-areas, which are generally less than 10 acres in size. Assign upstream and downstream node numbers to each sub-area.
2. Estimate an initial T_c by using the appropriate nomograph or overland flow velocity estimation. The minimum T_c considered is 5.0 minutes.
3. Using the initial T_c , determine the corresponding values of I . Then $Q = CIA$.
4. Using Q , estimate the travel time between this node and the next by Manning's equation as applied to particular channel or conduit linking the two nodes. Then, repeat the calculation for Q based on the revised intensity (which is a function of the revised time of concentration)

The nodes are joined together by links, which may be street gutter flows, drainage swales, drainage ditches, pipe flow, or various channel flows. The AES computer sub-area menu is as follows:

SUBAREA HYDROLOGIC PROCESS

1. Confluence analysis at node.
2. Initial sub-area analysis (including time of concentration calculation).
3. Pipe flow travel time (computer estimated).
4. Pipe flow travel time (user specified).
5. Trapezoidal channel travel time.
6. Street flow analysis through sub-area.
7. User-specified information at node.
8. Addition of sub-area runoff to main line.
9. V-gutter flow through area.
10. Copy main stream data to memory bank
11. Confluence main stream data with a memory bank
12. Clear a memory bank.
31. Compute pipe-flow travel time thru subarea using computer estimated pipe size.
51. Compute trapezoidal channel flow travel time thru subarea.
81. Addition of subarea to mainline peak flow.

At the confluence point of two or more basins, the following procedure is used to combine peak flow rates to account for differences in the basin's times of concentration. This adjustment is based on the assumption that each basin's hydrographs are triangular in shape.

1. If the collection streams have the same times of concentration, then the Q values are directly summed,

$$Q_p = Q_a + Q_b; T_p = T_a = T_b$$

2. If the collection streams have different times of concentration, the smaller of the tributary Q values may be adjusted as follows:
 - a. The most frequent case is where the collection stream with the longer time of concentration has the larger Q. The smaller Q value is adjusted by a ratio of rainfall intensities.

$$Q_p = Q_b + Q_a (I_b/I_a); T_p = T_a$$

- b. In some cases, the collection stream with the shorter time of concentration has the larger Q. Then the smaller Q is adjusted by a ratio of the T values.

$$Q_p = Q_b + Q_a (T_b/T_a); T_p = T_b$$

2.2 County of San Diego Criteria

As defined by the San Diego County Hydrology Manual (SDCHM) dated June 2003, the Rational Method is the preferred equation for determining the hydrologic characteristics of basins up to approximately one square mile in size. The County of San Diego has developed its own tables, nomographs, and methodologies for analyzing storm water runoff for areas within the county. The County has also developed precipitation isopluvial contour maps that show even lines of rainfall anticipated from a given storm event (i.e. 100-year, 6-hour storm).

One of the variables of the RM equation is the runoff coefficient, C. The runoff coefficient is dependent only upon land use and soil type and the County of San Diego has developed a table of Runoff Coefficients for Urban Areas to be applied to basin located within the County of San Diego. The table categorizes the land use, the associated development density (dwelling units per acre) and the percentage of impervious area. Each of the categories listed has an associated runoff coefficient, C, for each soil type class.

The County has also illustrated in detail the methodology for determining the Time of Concentration, in particular the Initial Time of Concentration (Ti). The County has adopted the Federal Aviation Agency's (FAA) overland time of flow equation. For this project, High Density Residential at 43 DU/acre maximum overland flow lengths are used. This equation essentially limits the flow path length for the initial time of concentration to lengths to 100 feet for slopes of 10% and greater and 95 feet for slopes up to 5%, and is dependent on land use and slope. See the "Rational Formula – Overland Time of Flow Nomograph," shown in Figure 3-3 or Table 3-2 of the San Diego County Hydrology Manual (June 2003).

The travel time (Tt) is computed by dividing the length of the flow path by the computed velocity. Figure 3-6 of the SDCHM is used to estimate time of travel for street gutter flow. Velocity in a channel is estimated by using the nomograph shown in Figure 3-7 (Manning's Equation Nomograph). Travel time in natural watersheds is calculated from the Kirpich nomograph in Figure 3-4 or from the Kirpich equation.

See Appendix B of this report for San Diego County Hydrology Manual reference material.

2.3 City of Encinitas Standards

The City of Encinitas Engineering Design Manual Chapter 6 and Appendix 6 has additional requirements for hydrology reports which are outlined in the Grading, Erosion and Sediment Control Ordinance. Please refer to this manual for further details. The drainage analysis used in this study is also consistent with the requirements set forth in Section 2.3 of the City of Encinitas Engineering Design Manual.

2.4 Runoff Coefficient Determination

In accordance with City of Encinitas Engineering Design Manual, runoff coefficients are based on land use and soil type. Per the City of Encinitas Engineering Manual the soil condition used in this study is assumed to be Type D. An appropriate area-weighted runoff coefficient (C) for each Drainage Basin A and B was calculated using the methodology presented in Chapter 6 of the City of Encinitas Engineering Design Manual. Impervious areas will use a runoff coefficient of 0.90 while pervious areas will use a runoff coefficient of 0.45. These coefficients are multiplied by the percentage of total area (A) included in that class. The sum of products for all land uses is the weighted runoff coefficient ($\sum[C]$). See the table below for weighted runoff coefficient “C” calculations. The Existing and Post-Development Hydrology Maps show the drainage basin subareas, on-site drainage system and nodal points.

$$\underline{\sum C} = \frac{C_1 A_1 + C_2 A_2}{A_1 + A_2}$$

Summary of Existing Condition Weighted Runoff Coefficients						
Drainage Basin	Total Area, A (ac)	C ₁	A ₁	C ₂	A ₂	C
A	2.48	0.9	0	0.45	2.48	0.45
B	5.89	0.9	0	0.45	5.89	0.45

Summary of Proposed Condition Weighted Runoff Coefficients						
Drainage Basin	Total Area, A (ac)	C ₁	A ₁	C ₂	A ₂	C
A	5.80	0.9	4.62	0.45	1.18	0.81
B	2.57	0.9	0	0.45	2.58	0.45

2.5 Hydraulics

The hydraulics of existing and proposed storm drain pipes were analyzed using the AES computer program. For pipe flow, a Manning's N value of 0.013 was used to reflect the use of HDPE and RCP pipe. All proposed storm drain pipes have been sized based on the proposed unmitigated flow condition for the 100-year storm event. Pipe, curb, gutter, curb inlet and catch basin capacity calculations are included in the Appendix of this report.

2.6 Detention Analysis

The HMP Biofiltration basins (BMP) provide pollutant control, hydromodification management flow control and mitigation of the 100-year storm event peak flow rate. The 100-year storm event detention analysis was performed using HydroCAD Stormwater Modeling software. The inflow runoff hydrographs to the BMPs were modeled using RatHydro which is a Rational Method Design Storm Hydrograph software that creates a hydrograph using the results of the Rational Method calculations. HydroCAD has the ability to route the 100-year 6-hour storm event inflow hydrographs through the BMPs and based on the BMP cross sectional geometry, stage storage and outlet structure data, HydroCAD calculates the detained peak flow rates and detained times to peak.

The detained flow rates and time of concentrations from the detention basins were then entered into the project's AES hydrologic study using Process Code 7 (see Section 2.1 of this report for summary of AES process codes). A mitigated condition AES report was produced for the 100-year storm event. See Appendix C for proposed mitigated condition hydrologic calculations. HydroCAD detention output reports will be provided upon final engineering.

The HMP Biofiltration facilities consists of a basin with 18 inches of engineered soil and Rtank structure storage layer of 6.5'. Runoff will be biofiltered through the engineered soil and gravel layers, then collected in a series of small PVC drainpipes and directed to a catch basin located in the HMP Biofiltration basin where runoff will be mitigated via a small HMP orifice to comply with HMP requirements. In larger storm events, runoff not filtered through the engineered soil and gravel layers will be conveyed via an overflow outlet structure. Runoff conveyed via the outlet structure will bypass the small HMP orifice and be conveyed directly to the proposed storm drain discharge pipe.

Based on the results of the HydroCAD analysis, the HMP Biofiltration facilities provide mitigation for the 100-year storm event peak flow rate, detaining the proposed condition.

APPENDIX A

Existing and Post Development Hydrology Node Maps

EXISTING CONDITION HYDROLOGY NODE MAP

PIRAEUS STREET, ENCINITAS, CA

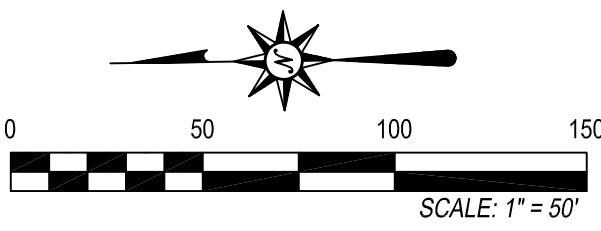


LEGEND

PROPERTY LINE	---
RIGHT-OF-WAY	---
ADJACENT PROPERTY LINE	---
CENTER LINE OF ROAD	---
DRAINAGE BOUNDARY	---
INITIAL SUB-BASIN BOUNDARY	---
DRAINAGE PATH OF TRAVEL	---
EXISTING CONTOURS	---
BASIN DESIGNATOR	---
BASIN INFORMATION	---
AREA (AC)	---
SUBAREA Q (CFS)	---

PLAN VIEW - EXISTING CONDITION HYDROLOGY

SCALE: 1" = 50'



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POST-DEVELOPEMENT HYDROLOGY NODE MAP

PIRAEUS STREET, ENCINITAS, CA



APPENDIX B

Hydrology Support Material

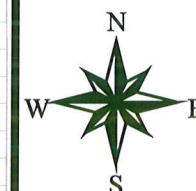
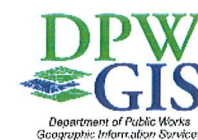
County of San Diego Hydrology Manual



Rainfall Isopluvials

100 Year Rainfall Event - 6 Hours

----- Isopluvial (inches)

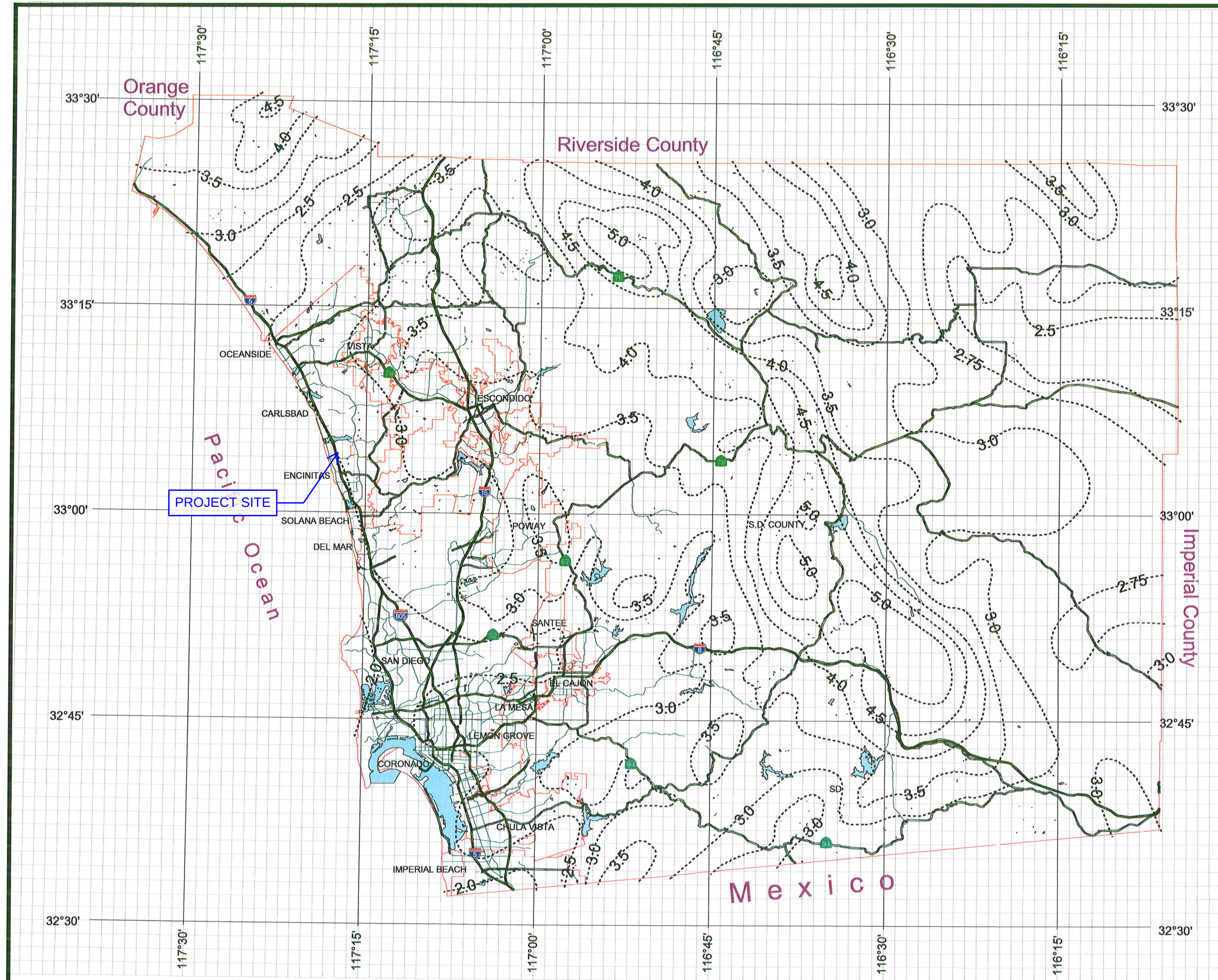


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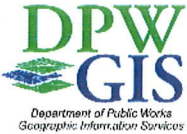
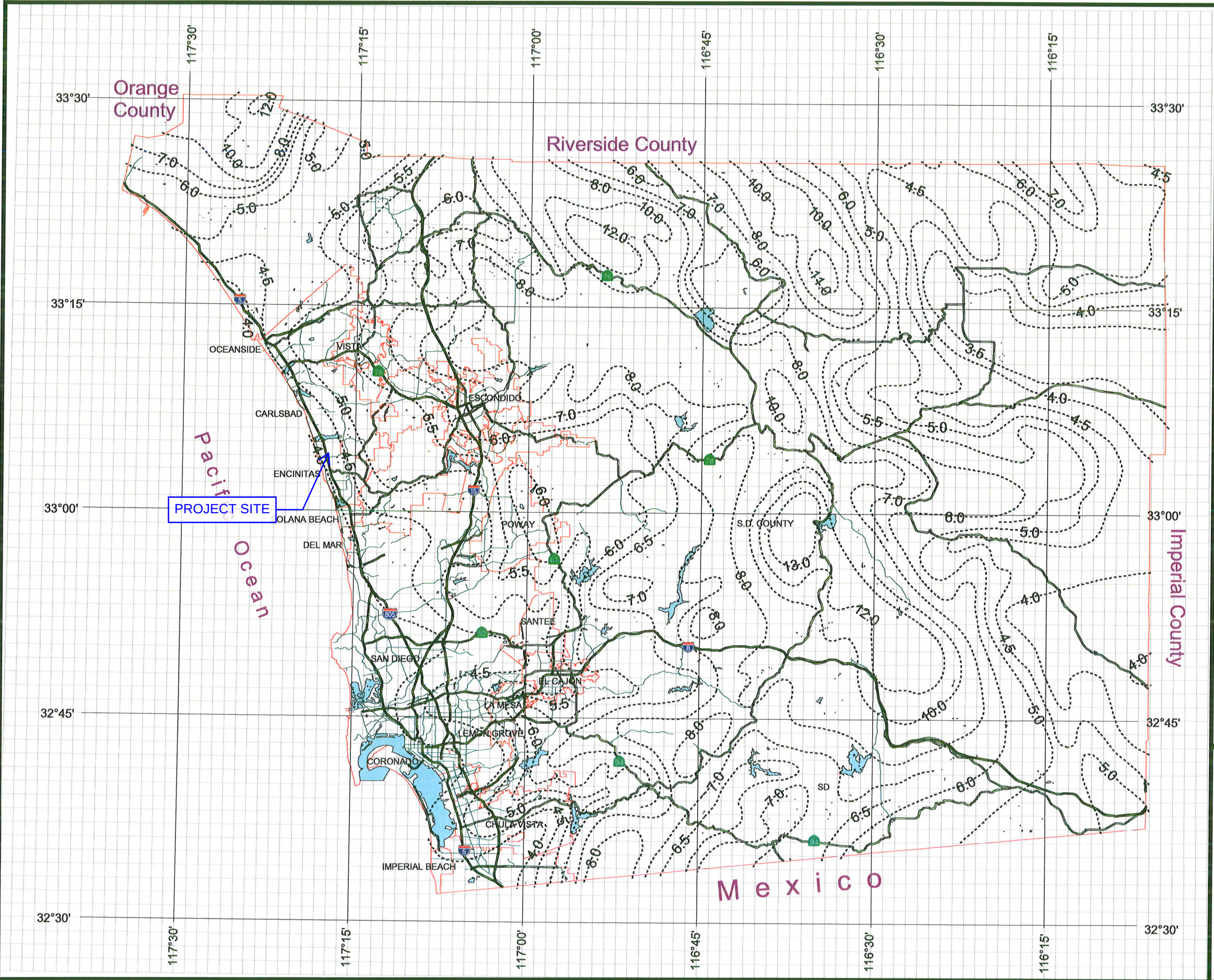
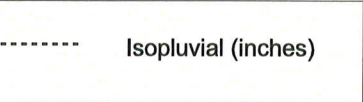


County of San Diego Hydrology Manual



Rainfall Isopluvials

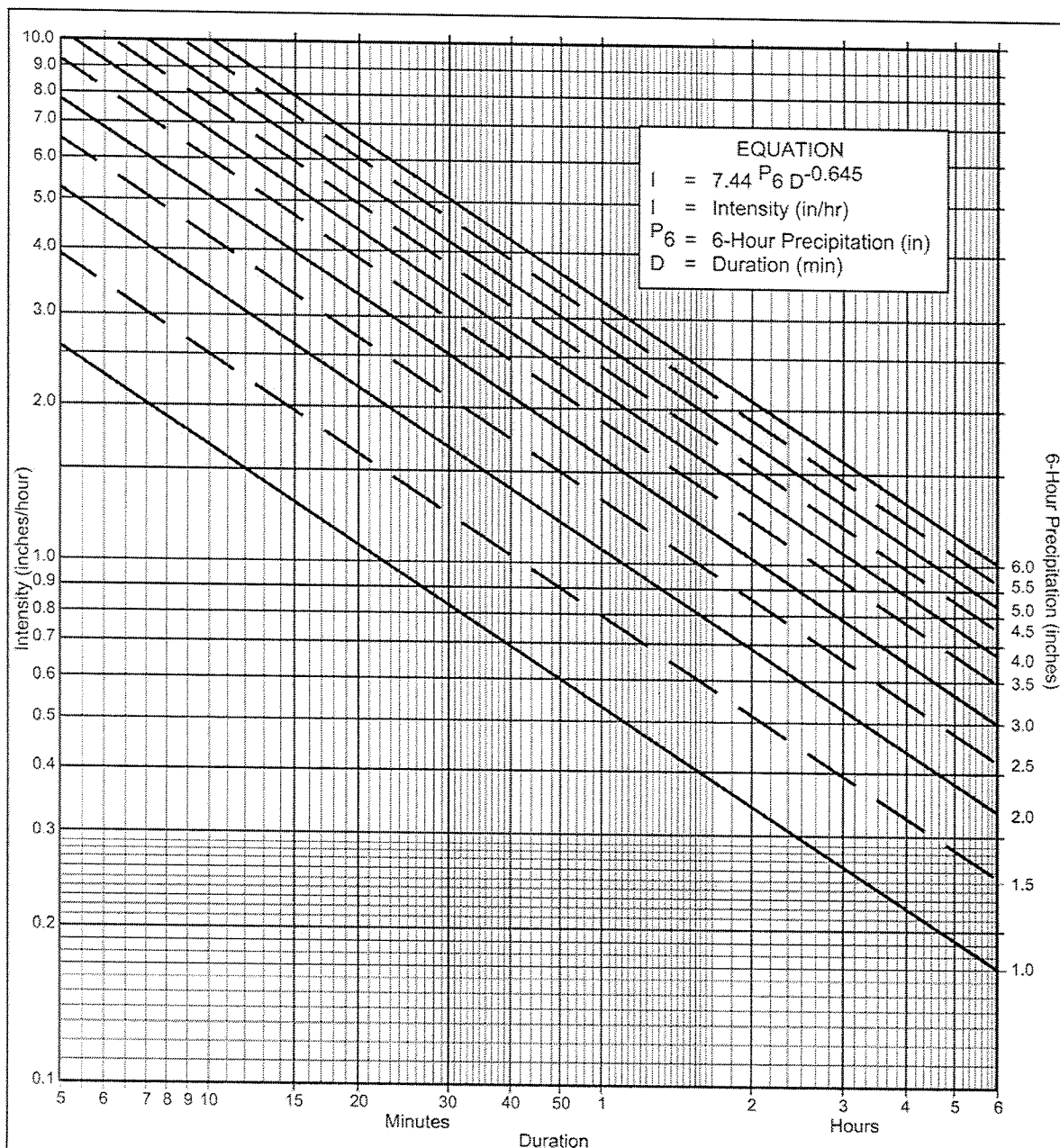
100 Year Rainfall Event - 24 Hours



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Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

Application Form:

- (a) Selected frequency 100 year
- (b) $P_6 = \underline{2.5}$ in., $P_{24} = \underline{4.2}$, $\frac{P_6}{P_{24}} = \underline{60} \%$ (2)
- (c) Adjusted $P_6^{(2)} = \underline{2.5}$ in.
- (d) $t_x = \underline{5.52}$ min.
- (e) $I = \underline{6.18}$ in./hr.

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

P6	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
Duration	I	I	I	I	I	I	I	I	I	I	I
5	2.63	3.95	5.27	6.59	7.90	9.22	10.54	11.86	13.17	14.49	15.81
7	2.12	3.18	4.24	5.30	6.36	7.42	8.48	9.54	10.60	11.66	12.72
10	1.68	2.53	3.37	4.21	5.05	5.90	6.74	7.58	8.42	9.27	10.11
15	1.30	1.95	2.59	3.24	3.89	4.54	5.19	5.84	6.49	7.13	7.78
20	1.08	1.62	2.15	2.69	3.23	3.77	4.31	4.85	5.39	5.93	6.46
25	0.93	1.40	1.87	2.33	2.80	3.27	3.73	4.20	4.67	5.13	5.60
30	0.83	1.24	1.66	2.07	2.49	2.90	3.32	3.73	4.15	4.56	4.98
40	0.59	1.03	1.38	1.72	2.07	2.41	2.76	3.10	3.45	3.79	4.13
50	0.50	0.90	1.19	1.49	1.79	2.09	2.39	2.69	2.98	3.28	3.58
60	0.53	0.80	1.06	1.33	1.59	1.86	2.12	2.39	2.65	2.92	3.18
90	0.41	0.61	0.82	1.02	1.23	1.43	1.63	1.84	2.04	2.25	2.45
120	0.34	0.51	0.68	0.85	1.02	1.19	1.36	1.53	1.70	1.87	2.04
150	0.29	0.44	0.59	0.73	0.88	1.03	1.18	1.32	1.47	1.62	1.76
180	0.26	0.39	0.52	0.65	0.78	0.91	1.04	1.18	1.31	1.44	1.57
240	0.22	0.33	0.43	0.54	0.65	0.76	0.87	0.98	1.08	1.19	1.30
300	0.19	0.28	0.38	0.47	0.56	0.66	0.75	0.85	0.94	1.03	1.13
360	0.17	0.25	0.33	0.42	0.50	0.58	0.67	0.75	0.84	0.92	1.00

Intensity-Duration Design Chart - Template

FIGURE

3-1

Note that the Initial Time of Concentration should be reflective of the general land-use at the upstream end of a drainage basin. A single lot with an area of two or less acres does not have a significant effect where the drainage basin area is 20 to 600 acres.

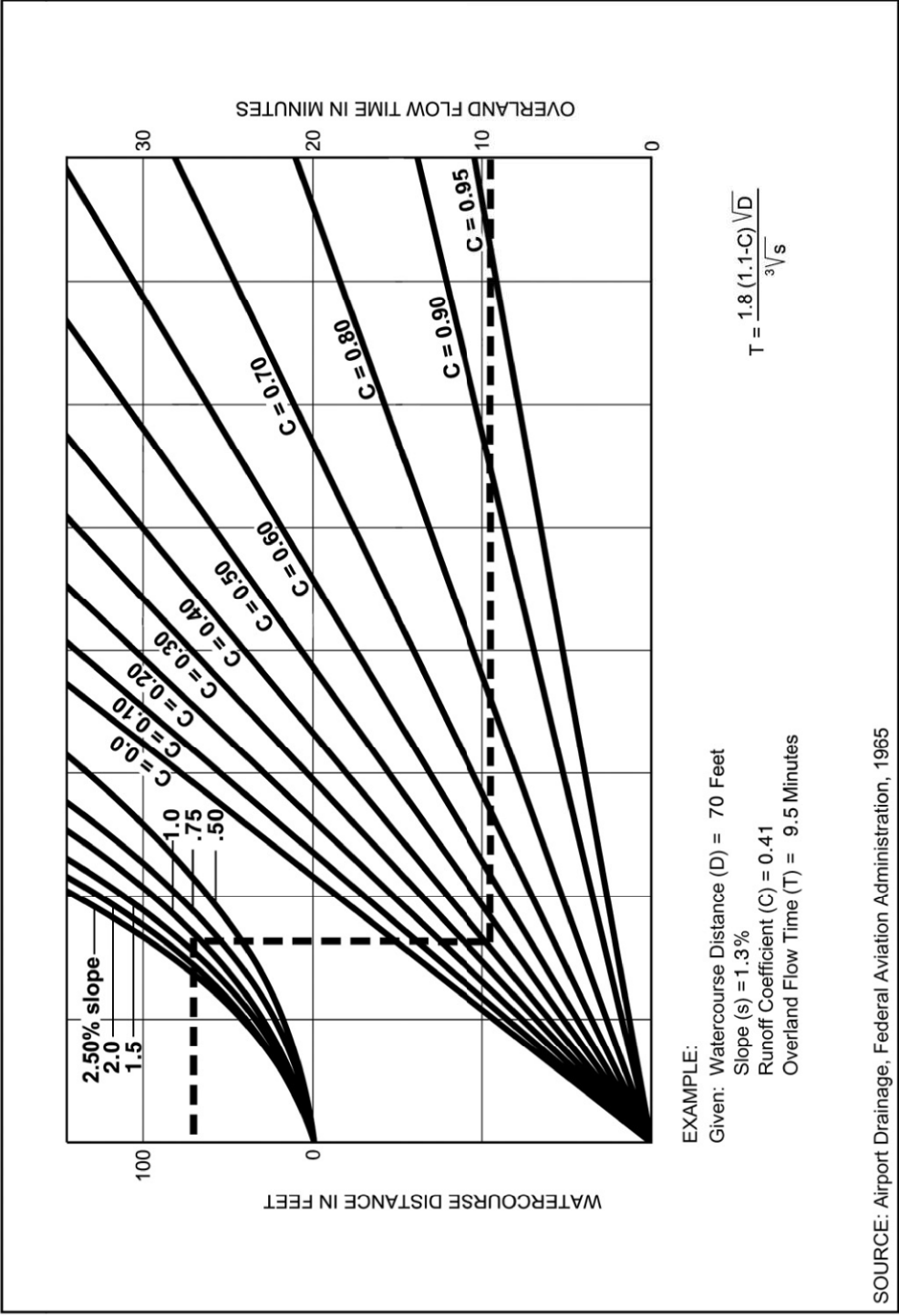
Table 3-2 provides limits of the length (Maximum Length (L_M)) of sheet flow to be used in hydrology studies. Initial T_i values based on average C values for the Land Use Element are also included. These values can be used in planning and design applications as described below. Exceptions may be approved by the “Regulating Agency” when submitted with a detailed study.

Table 3-2

**MAXIMUM OVERLAND FLOW LENGTH (L_M)
& INITIAL TIME OF CONCENTRATION (T_i)**

Element*	DU/ Acre	.5%		1%		2%		3%		5%		10%	
		L_M	T_i	L_M	T_i	L_M	T_i	L_M	T_i	L_M	T_i	L_M	T_i
Natural		50	13.2	70	12.5	85	10.9	100	10.3	100	8.7	100	6.9
LDR	1	50	12.2	70	11.5	85	10.0	100	9.5	100	8.0	100	6.4
LDR	2	50	11.3	70	10.5	85	9.2	100	8.8	100	7.4	100	5.8
LDR	2.9	50	10.7	70	10.0	85	8.8	95	8.1	100	7.0	100	5.6
MDR	4.3	50	10.2	70	9.6	80	8.1	95	7.8	100	6.7	100	5.3
MDR	7.3	50	9.2	65	8.4	80	7.4	95	7.0	100	6.0	100	4.8
MDR	10.9	50	8.7	65	7.9	80	6.9	90	6.4	100	5.7	100	4.5
MDR	14.5	50	8.2	65	7.4	80	6.5	90	6.0	100	5.4	100	4.3
HDR	24	50	6.7	65	6.1	75	5.1	90	4.9	95	4.3	100	3.5
HDR	43	50	5.3	65	4.7	75	4.0	85	3.8	95	3.4	100	2.7
N. Com		50	5.3	60	4.5	75	4.0	85	3.8	95	3.4	100	2.7
G. Com		50	4.7	60	4.1	75	3.6	85	3.4	90	2.9	100	2.4
O.P./Com		50	4.2	60	3.7	70	3.1	80	2.9	90	2.6	100	2.2
Limited I.		50	4.2	60	3.7	70	3.1	80	2.9	90	2.6	100	2.2
General I.		50	3.7	60	3.2	70	2.7	80	2.6	90	2.3	100	1.9

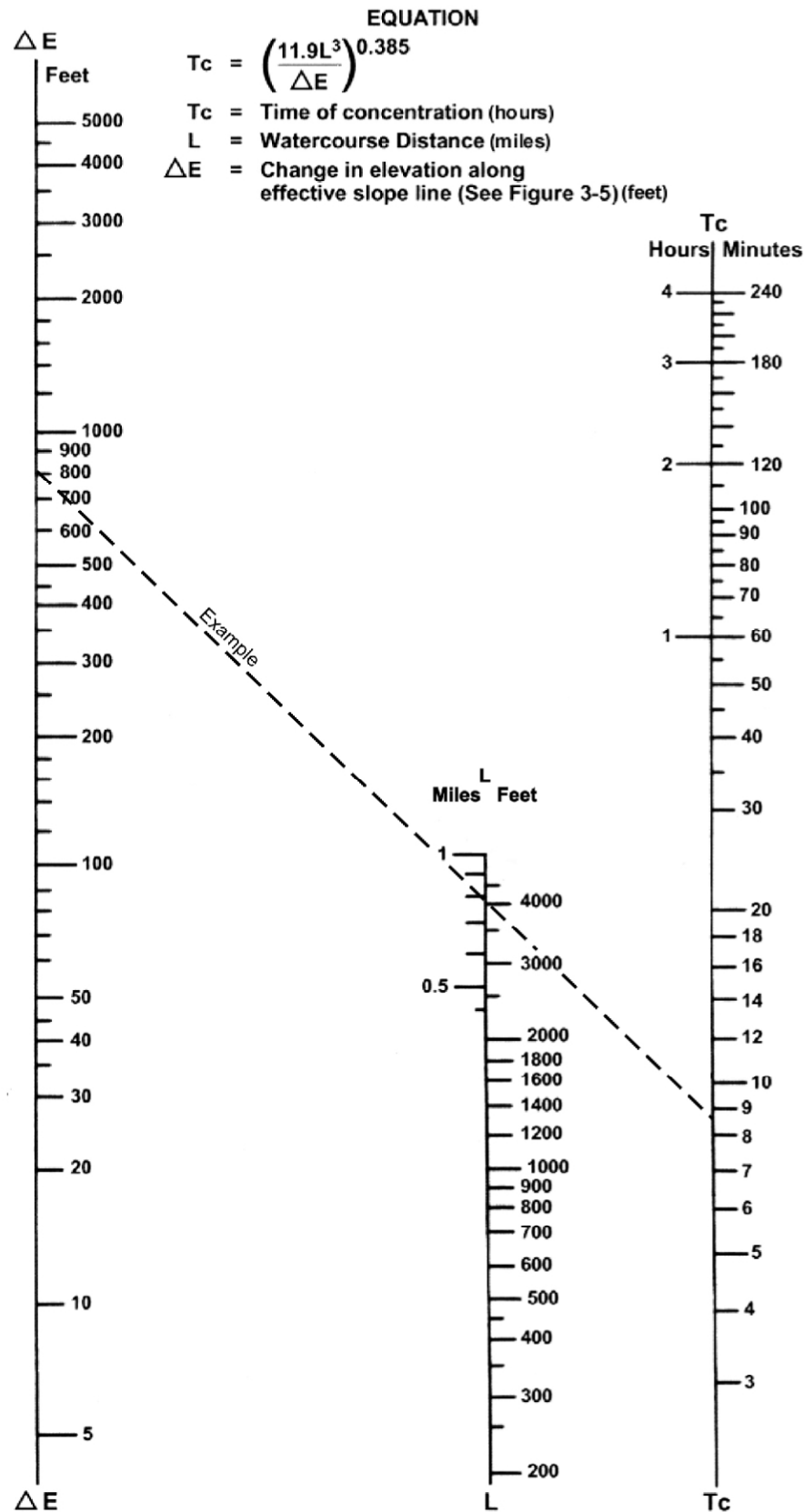
*See Table 3-1 for more detailed description



FIGURE

3-3

Rational Formula - Overland Time of Flow Nomograph

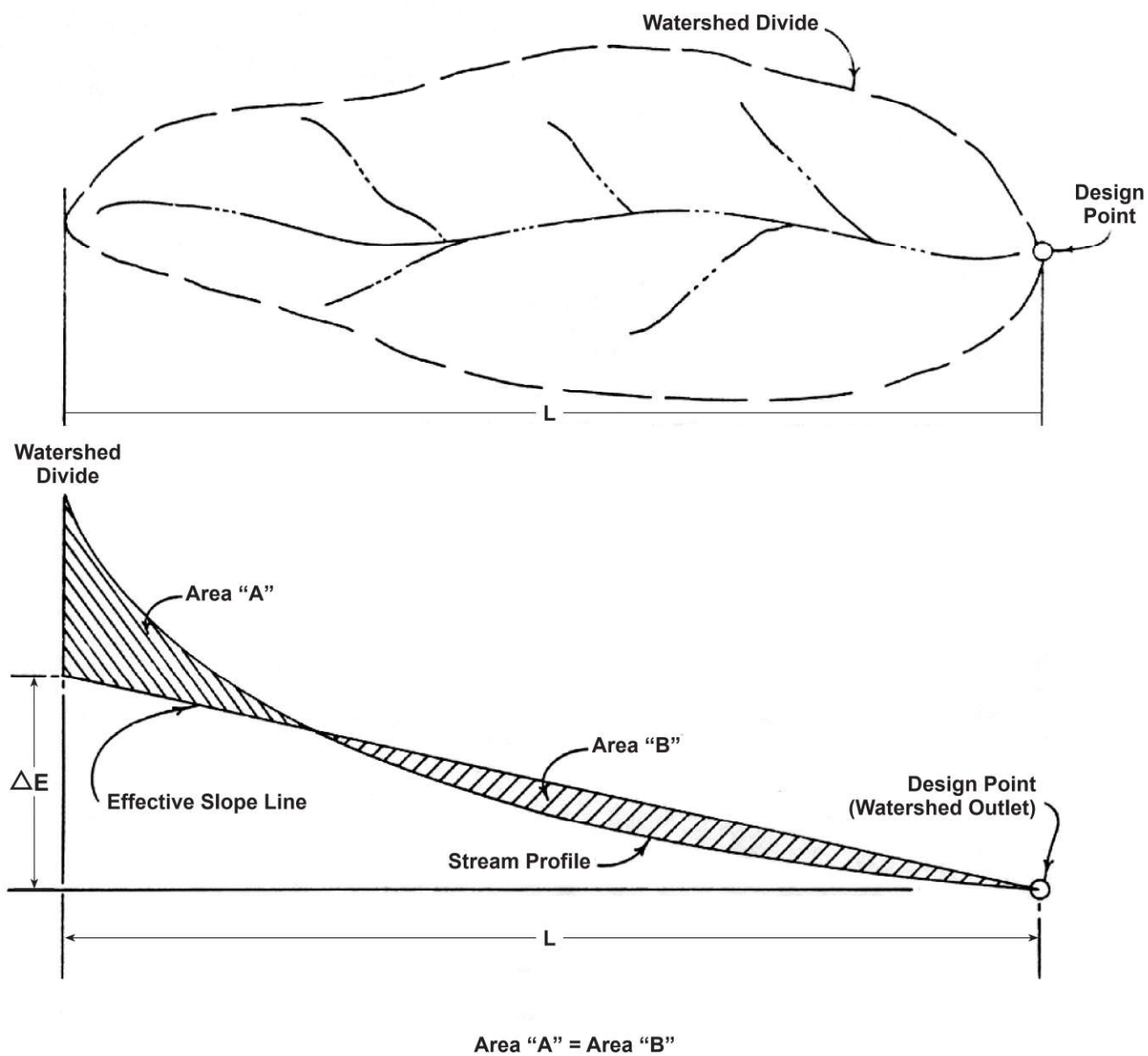


SOURCE: California Division of Highways (1941) and Kirpich (1940)

Nomograph for Determination of
Time of Concentration (T_c) or Travel Time (T_t) for Natural Watersheds

FIGURE

3-4

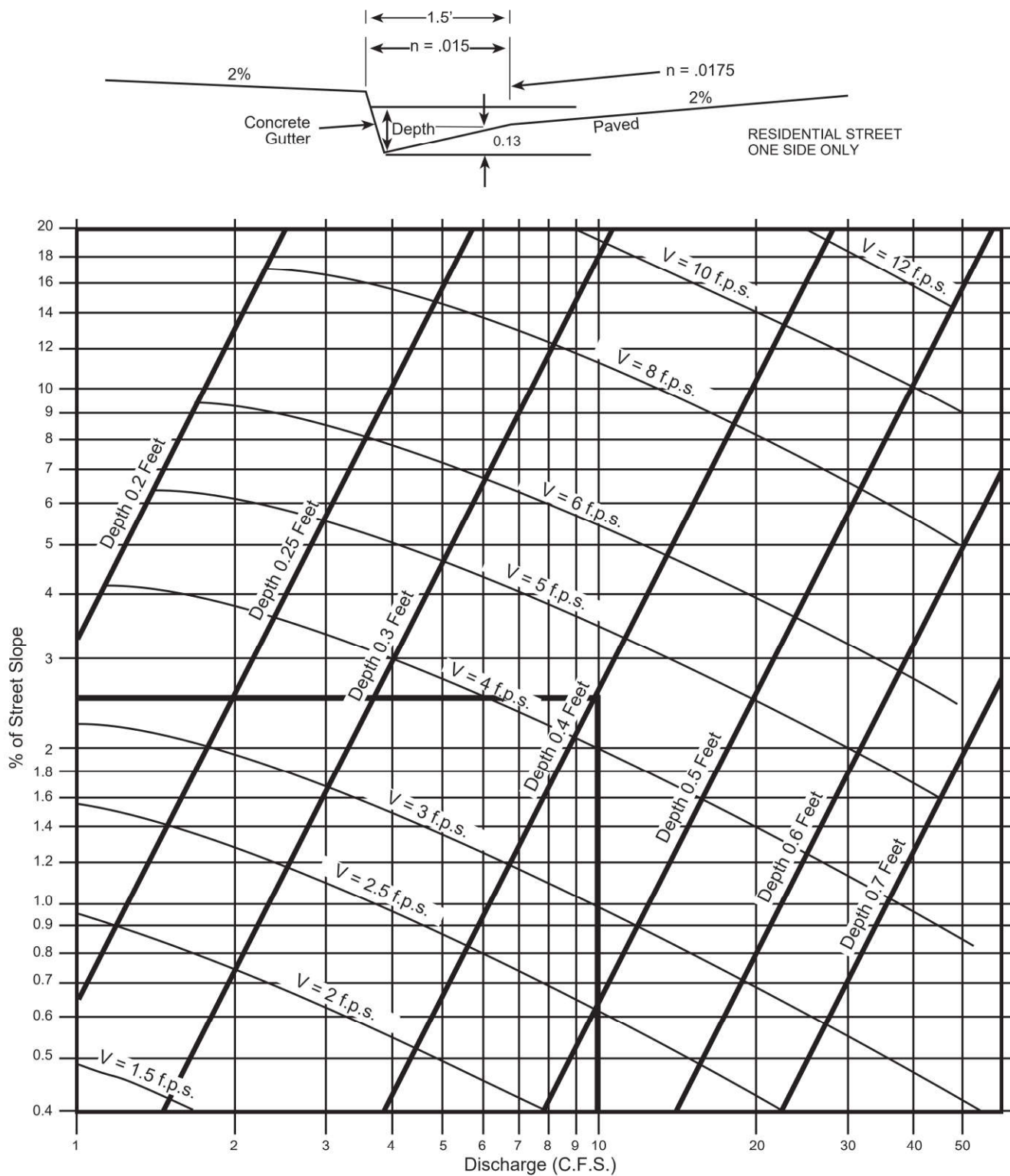


SOURCE: California Division of Highways (1941) and Kirpich (1940)

FIGURE

Computation of Effective Slope for Natural Watersheds

3-5



EXAMPLE:
 Given: $Q = 10$ $S = 2.5\%$
 Chart gives: Depth = 0.4, Velocity = 4.4 f.p.s.

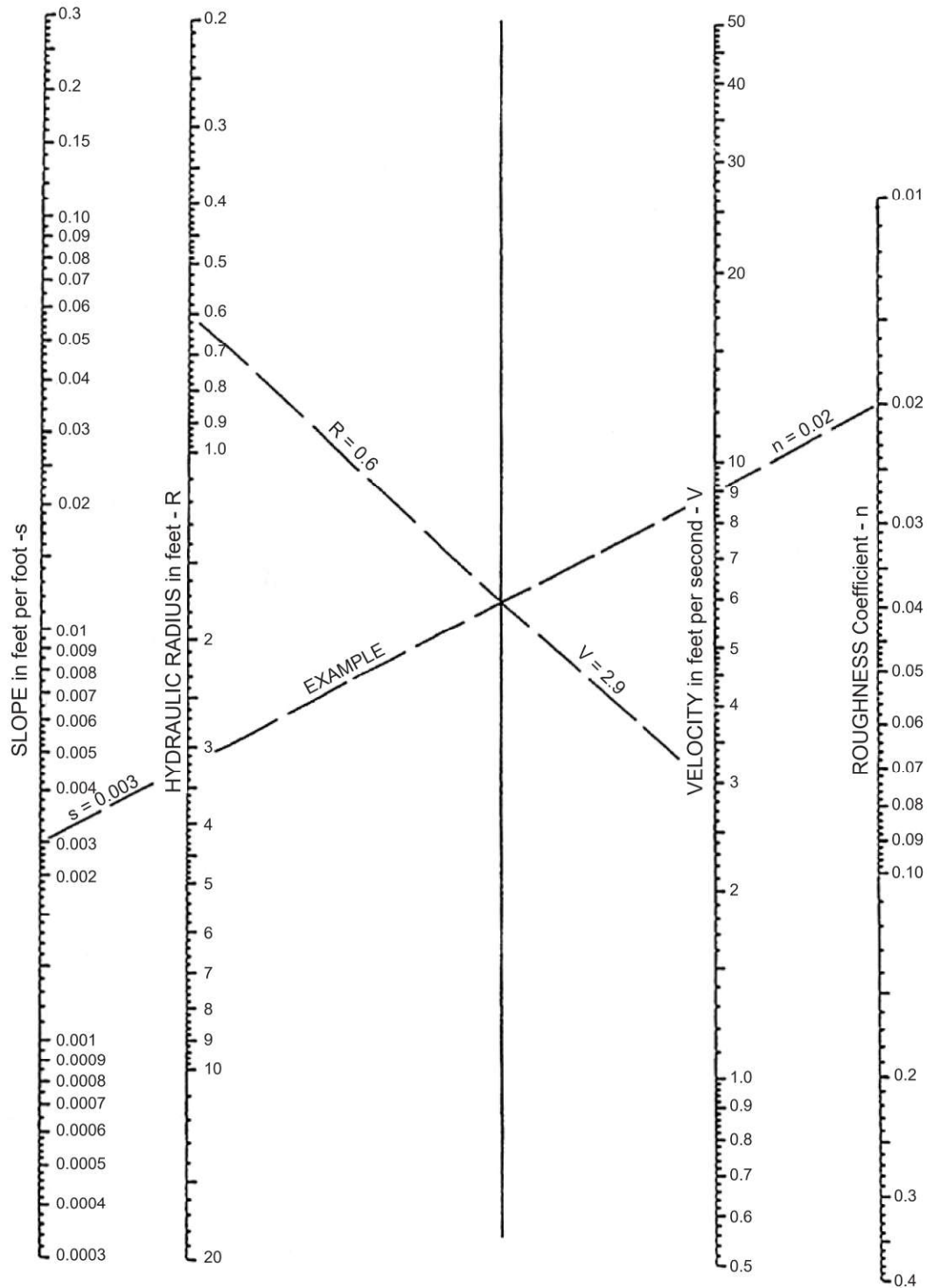
SOURCE: San Diego County Department of Special District Services Design Manual

Gutter and Roadway Discharge - Velocity Chart

FIGURE

3-6

$$\text{EQUATION: } V = \frac{1.49}{n} R^{2/3} s^{1/2}$$



GENERAL SOLUTION

SOURCE: USDOT, FHWA, HDS-3 (1961)

Manning's Equation Nomograph

FIGURE

3-7

Hydrologic Soil Group—San Diego County Area, California



**Natural Resources
Conservation Service**

Web Soil Survey
National Cooperative Soil Survey

3/29/2022
Page 1 of 4

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

Soil Rating Polygons

 A
 A/D
 B
 B/D
 C
 C/D
 D
 Not rated or not available

Soil Rating Lines

 A
 A/D
 B
 B/D
 C
 C/D
 D
 Not rated or not available

Soil Rating Points

 A
 A/D
 B
 B/D

 C
 C/D
 D
 Not rated or not available

Water Features

 Streams and Canals

Transportation

 Rails
 Interstate Highways
 US Routes
 Major Roads
 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: San Diego County Area, California
 Survey Area Data: Version 16, Sep 13, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jan 23, 2020—Feb 13, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

APPENDIX C

AES Existing Condition and Post-Development Output Reports

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1452

Analysis prepared by:

PASCO LARET SUITER & ASSOCIATES
1911 SAN DIEGO AVE. SUITE 100
SAN DIEGO, CA 92110

***** DESCRIPTION OF STUDY *****
* PIRAEUS STREET, ENCINITAS *
* PRE-DEVELOPMENT ANALYSIS *
* *

FILE NAME: 3733PRE.DAT
TIME/DATE OF STUDY: 09:47 09/02/2022

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 2.500
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
NO.	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

+-----+

| BEGIN FLOWS TO POC-B |

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 182.30

DOWNSTREAM ELEVATION(FEET) = 174.40

ELEVATION DIFFERENCE(FEET) = 7.90

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.629

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.102

SUBAREA RUNOFF(CFS) = 0.47

TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.47

FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 174.40 DOWNSTREAM(FEET) = 80.34

CHANNEL LENGTH THRU SUBAREA(FEET) = 1348.00 CHANNEL SLOPE = 0.0698

CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 10.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 0.50

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.839

*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.62

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.80

AVERAGE FLOW DEPTH(FEET) = 0.21 TRAVEL TIME(MIN.) = 5.92

Tc(MIN.) = 11.55

SUBAREA AREA(ACRES) = 5.72 SUBAREA RUNOFF(CFS) = 9.88

AREA-AVERAGE RUNOFF COEFFICIENT = 0.450

TOTAL AREA(ACRES) = 5.9 PEAK FLOW RATE(CFS) = 10.17

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.29 FLOW VELOCITY(FEET/SEC.) = 4.54

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 1443.00 FEET.

| END FLOWS TO POC-B |

BEGIN FLOWS TO POC-A

FLOW PROCESS FROM NODE 200.00 TO NODE 101.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 182.30

DOWNSTREAM ELEVATION(FEET) = 173.36

ELEVATION DIFFERENCE(FEET) = 8.94

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.402

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.266

SUBAREA RUNOFF(CFS) = 0.28

TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.28

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 173.36 DOWNSTREAM(FEET) = 106.30

CHANNEL LENGTH THRU SUBAREA(FEET) = 631.00 CHANNEL SLOPE = 0.1063

CHANNEL BASE(FEET) = 15.00 "Z" FACTOR = 8.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.50

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.389

*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.70

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.64

AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 3.98

Tc(MIN.) = 9.38

SUBAREA AREA(ACRES) = 2.38 SUBAREA RUNOFF(CFS) = 4.70

AREA-AVERAGE RUNOFF COEFFICIENT = 0.450

TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 4.90

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 3.29
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 102.00 = 726.00 FEET.

END FLOWS TO POC-A

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.5 TC(MIN.) = 9.38

PEAK FLOW RATE(CFS) = 4.90

END OF RATIONAL METHOD ANALYSIS



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1452

Analysis prepared by:

PASCO LARET SUITER & ASSOCIATES
1911 SAN DIEGO AVE. SUITE 100
SAN DIEGO, CA 92110

***** DESCRIPTION OF STUDY *****
* PIRAEUS STREET, ENCINITAS *
* POST-DEVELOPMENT UNMITIGATED ANALYSIS *
* *

FILE NAME: 3733PSTU.DAT
TIME/DATE OF STUDY: 12:09 09/08/2022

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 2.500
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	12.0	1.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

+-----+

BEGIN FLOWS TO POC-B

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 174.70

DOWNSTREAM ELEVATION(FEET) = 142.09

ELEVATION DIFFERENCE(FEET) = 32.61

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.431

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.245

SUBAREA RUNOFF(CFS) = 0.67

TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.67

FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 142.09 DOWNSTREAM(FEET) = 80.34

CHANNEL LENGTH THRU SUBAREA(FEET) = 492.00 CHANNEL SLOPE = 0.1255

CHANNEL BASE(FEET) = 3.50 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 28.50

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.099

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.82

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.09

AVERAGE FLOW DEPTH(FEET) = 0.12 TRAVEL TIME(MIN.) = 2.01

Tc(MIN.) = 7.44

SUBAREA AREA(ACRES) = 0.99 SUBAREA RUNOFF(CFS) = 2.27

AREA-AVERAGE RUNOFF COEFFICIENT = 0.450

TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 2.82

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 4.76

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 592.00 FEET.

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 5
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 7.44
RAINFALL INTENSITY(INCH/HR) = 5.10
TOTAL STREAM AREA(ACRES) = 1.23
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.82

FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 108.00
DOWNSTREAM ELEVATION(FEET) = 95.20
ELEVATION DIFFERENCE(FEET) = 12.80
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.431
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN T_c CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.245
SUBAREA RUNOFF(CFS) = 0.14
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.14

FLOW PROCESS FROM NODE 204.00 TO NODE 202.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 95.20 DOWNSTREAM(FEET) = 80.34
CHANNEL LENGTH THRU SUBAREA(FEET) = 790.00 CHANNEL SLOPE = 0.0188
CHANNEL BASE(FEET) = 1.50 "Z" FACTOR = 12.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 0.50
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.328
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.72
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.47
AVERAGE FLOW DEPTH(FEET) = 0.15 TRAVEL TIME(MIN.) = 8.98
T_c(MIN.) = 14.41
SUBAREA AREA(ACRES) = 0.75 SUBAREA RUNOFF(CFS) = 1.12
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 1.20

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.19 FLOW VELOCITY(FEET/SEC.) = 1.62

LONGEST FLOWPATH FROM NODE 203.00 TO NODE 202.00 = 890.00 FEET.

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 5

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 14.41

RAINFALL INTENSITY(INCH/HR) = 3.33

TOTAL STREAM AREA(ACRES) = 0.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.20

FLOW PROCESS FROM NODE 153.00 TO NODE 153.00 IS CODE = 81

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.328

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.5036

SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.38

TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 1.58

TC(MIN.) = 14.41

FLOW PROCESS FROM NODE 153.00 TO NODE 500.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 93.00 DOWNSTREAM(FEET) = 90.52

FLOW LENGTH(FEET) = 29.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 6.0 INCH PIPE IS 4.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 9.29

ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.58

PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 14.46

LONGEST FLOWPATH FROM NODE 0.00 TO NODE 500.00 = 29.00 FEET.

FLOW PROCESS FROM NODE 500.00 TO NODE 202.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 90.52 DOWNSTREAM ELEVATION(FEET) = 80.34
STREET LENGTH(FEET) = 333.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.59
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.25
HALFSTREET FLOOD WIDTH(FEET) = 6.21
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.15
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.79
STREET FLOW TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 16.23
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.083

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.507
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.02
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 1.58

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.21
FLOW VELOCITY(FEET/SEC.) = 3.12 DEPTH*VELOCITY(FT*FT/SEC.) = 0.78
LONGEST FLOWPATH FROM NODE 0.00 TO NODE 202.00 = 362.00 FEET.

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 5
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 16.23
RAINFALL INTENSITY(INCH/HR) = 3.08
TOTAL STREAM AREA(ACRES) = 0.95
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.58

FLOW PROCESS FROM NODE 154.00 TO NODE 154.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

```
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.083
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5458
SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.35
TOTAL AREA(ACRES) = 1.1 TOTAL RUNOFF(CFS) = 1.83
TC(MIN.) = 16.23
```

FLOW PROCESS FROM NODE 154.00 TO NODE 202.00 IS CODE = 51

```
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
```

```
ELEVATION DATA: UPSTREAM(FEET) = 90.00 DOWNSTREAM(FEET) = 80.34
CHANNEL LENGTH THRU SUBAREA(FEET) = 114.00 CHANNEL SLOPE = 0.0847
CHANNEL BASE(FEET) = 2.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.048
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.85
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.57
AVERAGE FLOW DEPTH(FEET) = 0.12 TRAVEL TIME(MIN.) = 0.29
Tc(MIN.) = 16.52
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.02
AREA-AVERAGE RUNOFF COEFFICIENT = 0.548
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 1.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 6.54
LONGEST FLOWPATH FROM NODE 0.00 TO NODE 202.00 = 114.00 FEET.
```

```
+-----+
| ADD SUBAREA B-7 AT NODE 510 |
|                               |
+-----+
```

FLOW PROCESS FROM NODE 510.00 TO NODE 510.00 IS CODE = 81

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-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
```

```
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.048
*USER SPECIFIED(SUBAREA):
```

USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5378
SUBAREA AREA(ACRES) = 0.13 SUBAREA RUNOFF(CFS) = 0.18
TOTAL AREA(ACRES) = 1.2 TOTAL RUNOFF(CFS) = 2.02
TC(MIN.) = 16.52

FLOW PROCESS FROM NODE 510.00 TO NODE 143.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 64.00
UPSTREAM ELEVATION(FEET) = 150.50
DOWNSTREAM ELEVATION(FEET) = 127.00
ELEVATION DIFFERENCE(FEET) = 23.50
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.345
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN T_c CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON T_c = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.12
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.12

FLOW PROCESS FROM NODE 143.00 TO NODE 145.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 127.00 DOWNSTREAM(FEET) = 111.34
CHANNEL LENGTH THRU SUBAREA(FEET) = 180.00 CHANNEL SLOPE = 0.0870
CHANNEL BASE(FEET) = 2.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.354

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.27
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.18
AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 0.94
T_c(MIN.) = 5.29
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.31
AREA-AVERAGE RUNOFF COEFFICIENT = 0.666
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.42

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 3.98

LONGEST FLOWPATH FROM NODE 510.00 TO NODE 145.00 = 244.00 FEET.

FLOW PROCESS FROM NODE 145.00 TO NODE 202.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 111.34 DOWNSTREAM ELEVATION(FEET) = 80.34

STREET LENGTH(FEET) = 1213.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.44

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.17

HALFSTREET FLOOD WIDTH(FEET) = 2.13

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.68

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.45

STREET FLOW TRAVEL TIME(MIN.) = 7.55 Tc(MIN.) = 12.84

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.585

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.679

SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.03

TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.42

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.16 HALFSTREET FLOOD WIDTH(FEET) = 1.50

FLOW VELOCITY(FEET/SEC.) = 3.02 DEPTH*VELOCITY(FT*FT/SEC.) = 0.47

LONGEST FLOWPATH FROM NODE 510.00 TO NODE 202.00 = 1457.00 FEET.

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 5

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 5 ARE:

TIME OF CONCENTRATION(MIN.) = 12.84

RAINFALL INTENSITY(INCH/HR) = 3.58
TOTAL STREAM AREA(ACRES) = 0.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.42

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.82	7.44	5.099	1.23
2	1.20	14.41	3.328	0.80
3	1.58	16.23	3.083	0.95
5	0.42	12.84	3.585	0.11

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 5 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	0.00	0.00	6.587
2	4.41	7.44	5.099
3	4.72	12.84	3.585
4	4.83	14.41	3.328
5	4.76	16.23	3.083

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.83 Tc(MIN.) = 14.41
TOTAL AREA(ACRES) = 3.1
LONGEST FLOWPATH FROM NODE 510.00 TO NODE 202.00 = 1457.00 FEET.

```
+-----+
| END FLOWS TO POC-B |
|                     |
+-----+
```

```
+-----+
| BEGIN FLOWS TO POC-A |
|                     |
+-----+
```

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

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-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
```

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00

UPSTREAM ELEVATION(FEET) = 181.00
DOWNSTREAM ELEVATION(FEET) = 172.00
ELEVATION DIFFERENCE(FEET) = 9.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.625
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.16

FLOW PROCESS FROM NODE 101.00 TO NODE 151.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 156.53 DOWNSTREAM(FEET) = 156.00
FLOW LENGTH(FEET) = 10.50 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 6.000
DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.39
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.16
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 1.67
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 151.00 = 55.50 FEET.

FLOW PROCESS FROM NODE 151.00 TO NODE 102.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 156.00 DOWNSTREAM ELEVATION(FEET) = 138.54
STREET LENGTH(FEET) = 321.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.35
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.26
HALFSTREET FLOOD WIDTH(FEET) = 6.58
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.26

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.10
STREET FLOW TRAVEL TIME(MIN.) = 1.26 Tc(MIN.) = 2.92
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.82 SUBAREA RUNOFF(CFS) = 4.37
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 4.54

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.96
FLOW VELOCITY(FEET/SEC.) = 4.93 DEPTH*VELOCITY(FT*FT/SEC.) = 1.50
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 376.50 FEET.

FLOW PROCESS FROM NODE 102.00 TO NODE 114.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	128.34	DOWNSTREAM(FEET) =	128.12
FLOW LENGTH(FEET) =	4.50	MANNING'S N =	0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS	6.6 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	10.19		
ESTIMATED PIPE DIAMETER(INCH) =	12.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	4.54		
PIPE TRAVEL TIME(MIN.) =	0.01	Tc(MIN.) =	2.93
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 114.00 =	381.00 FEET.		

FLOW PROCESS FROM NODE 114.00 TO NODE 114.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 150.62
DOWNSTREAM ELEVATION(FEET) = 146.63
ELEVATION DIFFERENCE(FEET) = 3.99
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.086

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
 THE MAXIMUM OVERLAND FLOW LENGTH = 91.00
 (Reference: Table 3-1B of Hydrology Manual)
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) = 0.69
 TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.69

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 62

 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<
 =====

UPSTREAM ELEVATION(FEET) = 146.63 DOWNSTREAM ELEVATION(FEET) = 140.51
 STREET LENGTH(FEET) = 97.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.17
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.21
 HALFSTREET FLOOD WIDTH(FEET) = 4.13
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.06
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
 STREET FLOW TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 3.48
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100
 S.C.S. CURVE NUMBER (AMC II) = 0
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
 SUBAREA AREA(ACRES) = 0.18 SUBAREA RUNOFF(CFS) = 0.96
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.65

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.17
 FLOW VELOCITY(FEET/SEC.) = 4.29 DEPTH*VELOCITY(FT*FT/SEC.) = 0.98
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 105.00 = 192.00 FEET.

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 137.51 DOWNSTREAM(FEET) = 133.85
FLOW LENGTH(FEET) = 82.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.67
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.65
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 3.66
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 106.00 = 274.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 3.66
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.65

FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 146.18
DOWNSTREAM ELEVATION(FEET) = 140.74
ELEVATION DIFFERENCE(FEET) = 5.44
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.844
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.96

FLOW PROCESS FROM NODE 108.00 TO NODE 106.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 140.74 DOWNSTREAM ELEVATION(FEET) = 136.85
STREET LENGTH(FEET) = 70.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.36
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.22
HALFSTREET FLOOD WIDTH(FEET) = 4.80
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.90
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.87
STREET FLOW TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 3.14
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.15 SUBAREA RUNOFF(CFS) = 0.80
TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.76

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 5.62
FLOW VELOCITY(FEET/SEC.) = 4.06 DEPTH*VELOCITY(FT*FT/SEC.) = 0.97
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 106.00 = 165.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.14
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.33
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.76

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
------------------	-----------------	--------------	--------------------------	----------------

1	1.65	3.66	6.587	0.31
2	1.76	3.14	6.587	0.33

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.18	3.14	6.587
2	3.41	3.66	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.41 Tc(MIN.) = 3.66

TOTAL AREA(ACRES) = 0.6

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 106.00 = 274.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 109.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 133.85 DOWNSTREAM(FEET) = 131.86

FLOW LENGTH(FEET) = 199.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.03

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.41

PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 4.32

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 109.00 = 473.00 FEET.

FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 131.86 DOWNSTREAM(FEET) = 129.61

FLOW LENGTH(FEET) = 78.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.78

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.41

PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 4.49

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 110.00 = 551.00 FEET.

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.49
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.64
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.41
```

FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 142.09
DOWNSTREAM ELEVATION(FEET) = 136.65
ELEVATION DIFFERENCE(FEET) = 5.44
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.844
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.96
```

FLOW PROCESS FROM NODE 112.00 TO NODE 113.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

```
=====
UPSTREAM ELEVATION(FEET) = 136.65 DOWNSTREAM ELEVATION(FEET) = 134.29
STREET LENGTH(FEET) = 41.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00
```

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.28
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.22
HALFSTREET FLOOD WIDTH(FEET) = 4.58

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.91
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
 STREET FLOW TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 3.02
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100
 S.C.S. CURVE NUMBER (AMC II) = 0
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
 SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 0.64
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.60

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.25
 FLOW VELOCITY(FEET/SEC.) = 4.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.94
 LONGEST FLOWPATH FROM NODE 111.00 TO NODE 113.00 = 136.00 FEET.

 FLOW PROCESS FROM NODE 113.00 TO NODE 110.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
 ELEVATION DATA: UPSTREAM(FEET) = 131.29 DOWNSTREAM(FEET) = 129.61
 FLOW LENGTH(FEET) = 168.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 7.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.16
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 1.60
 PIPE TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 3.69
 LONGEST FLOWPATH FROM NODE 111.00 TO NODE 110.00 = 304.00 FEET.

 FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 3.69
 RAINFALL INTENSITY(INCH/HR) = 6.59
 TOTAL STREAM AREA(ACRES) = 0.30
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.60

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.41	4.49	6.587	0.64
2	1.60	3.69	6.587	0.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.02	3.69	6.587
2	5.02	4.49	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.02 Tc(MIN.) = 4.49
TOTAL AREA(ACRES) = 0.9
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 110.00 = 551.00 FEET.

FLOW PROCESS FROM NODE 110.00 TO NODE 114.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 129.61 DOWNSTREAM(FEET) = 128.12
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.55
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.02
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 4.59
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 114.00 = 601.00 FEET.

FLOW PROCESS FROM NODE 114.00 TO NODE 114.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	5.02	4.59	6.587	0.94

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 114.00 = 601.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.54	2.93	6.587	0.85

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 114.00 = 381.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM	RUNOFF	Tc	INTENSITY
--------	--------	----	-----------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)
1	7.74	2.93	6.587
2	9.55	4.59	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.55 Tc(MIN.) = 4.59
TOTAL AREA(ACRES) = 1.8

FLOW PROCESS FROM NODE 114.00 TO NODE 114.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

FLOW PROCESS FROM NODE 114.00 TO NODE 115.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 128.12 DOWNSTREAM(FEET) = 127.37
FLOW LENGTH(FEET) = 24.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.19
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.55
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 4.63
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 115.00 = 625.00 FEET.

FLOW PROCESS FROM NODE 115.00 TO NODE 115.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.63
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 1.79
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.55

FLOW PROCESS FROM NODE 116.00 TO NODE 530.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 30.00

UPSTREAM ELEVATION(FEET) = 138.00
DOWNSTREAM ELEVATION(FEET) = 136.30
ELEVATION DIFFERENCE(FEET) = 1.70
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.604
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.32
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.32

FLOW PROCESS FROM NODE 530.00 TO NODE 117.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	136.30	DOWNSTREAM ELEVATION(FEET) =	131.74
STREET LENGTH(FEET) =	78.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	12.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.80
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.19
HALFSTREET FLOOD WIDTH(FEET) = 3.02
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.82
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.71
STREET FLOW TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 1.94
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.18 SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 1.28

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.22 HALFSTREET FLOOD WIDTH(FEET) = 4.51
FLOW VELOCITY(FEET/SEC.) = 3.99 DEPTH*VELOCITY(FT*FT/SEC.) = 0.86
LONGEST FLOWPATH FROM NODE 116.00 TO NODE 117.00 = 108.00 FEET.

FLOW PROCESS FROM NODE 117.00 TO NODE 115.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 128.74 DOWNSTREAM(FEET) = 127.37
FLOW LENGTH(FEET) = 137.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.05
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.28
PIPE TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 2.51
LONGEST FLOWPATH FROM NODE 116.00 TO NODE 115.00 = 245.00 FEET.

FLOW PROCESS FROM NODE 115.00 TO NODE 155.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 2.51
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.24
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.28

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	9.55	4.63	6.587	1.79
2	1.28	2.51	6.587	0.24

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	6.46	2.51	6.587
2	10.83	4.63	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 10.83 Tc(MIN.) = 4.63
TOTAL AREA(ACRES) = 2.0
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 155.00 = 625.00 FEET.

FLOW PROCESS FROM NODE 115.00 TO NODE 118.00 IS CODE = 31

```

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 127.37 DOWNSTREAM(FEET) = 124.46
FLOW LENGTH(FEET) = 78.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 11.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.20
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.83
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 4.74
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 118.00 = 703.00 FEET.

*****
FLOW PROCESS FROM NODE 118.00 TO NODE 118.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.74
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 2.03
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.83

*****
FLOW PROCESS FROM NODE 119.00 TO NODE 120.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 93.00
UPSTREAM ELEVATION(FEET) = 133.92
DOWNSTREAM ELEVATION(FEET) = 128.64
ELEVATION DIFFERENCE(FEET) = 5.28
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.822
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.96

*****
FLOW PROCESS FROM NODE 120.00 TO NODE 118.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 125.64 DOWNSTREAM(FEET) = 124.46
FLOW LENGTH(FEET) = 118.00 MANNING'S N = 0.013

```

DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.82
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.96
PIPE TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 3.34
LONGEST FLOWPATH FROM NODE 119.00 TO NODE 118.00 = 211.00 FEET.

FLOW PROCESS FROM NODE 118.00 TO NODE 118.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.34
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.18
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.96

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	10.83	4.74	6.587	2.03
2	0.96	3.34	6.587	0.18

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.79	3.34	6.587
2	11.79	4.74	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.79 Tc(MIN.) = 4.74
TOTAL AREA(ACRES) = 2.2
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 118.00 = 703.00 FEET.

FLOW PROCESS FROM NODE 118.00 TO NODE 121.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 124.46 DOWNSTREAM(FEET) = 116.01
FLOW LENGTH(FEET) = 139.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.92

ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.79
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 4.91
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 121.00 = 842.00 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 121.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.91
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 2.21
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.79

FLOW PROCESS FROM NODE 156.00 TO NODE 123.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 143.00
DOWNSTREAM ELEVATION(FEET) = 138.63
ELEVATION DIFFERENCE(FEET) = 4.37
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.027
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
 THE MAXIMUM OVERLAND FLOW LENGTH = 93.00
 (Reference: Table 3-1B of Hydrology Manual)
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.91
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.91

FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 138.63 DOWNSTREAM ELEVATION(FEET) = 125.78
STREET LENGTH(FEET) = 245.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.75
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 7.18
AVERAGE FLOW VELOCITY(FT/SEC.) = 4.34
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.17
STREET FLOW TRAVEL TIME(MIN.) = 0.94 Tc(MIN.) = 3.97
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.69 SUBAREA RUNOFF(CFS) = 3.68
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 4.59

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.03
FLOW VELOCITY(FT/SEC.) = 4.91 DEPTH*VELOCITY(FT*FT/SEC.) = 1.51
LONGEST FLOWPATH FROM NODE 156.00 TO NODE 124.00 = 340.00 FEET.

FLOW PROCESS FROM NODE 124.00 TO NODE 121.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FT) = 116.23 DOWNSTREAM(FT) = 116.01
FLOW LENGTH(FT) = 4.50 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.7 INCHES
PIPE-FLOW VELOCITY(FT/SEC.) = 10.21
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.59
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 3.98
LONGEST FLOWPATH FROM NODE 156.00 TO NODE 121.00 = 344.50 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 121.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 3.98
 RAINFALL INTENSITY(INCH/HR) = 6.59
 TOTAL STREAM AREA(ACRES) = 0.86
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.59

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	11.79	4.91	6.587	2.21
2	4.59	3.98	6.587	0.86

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	16.38	3.98	6.587
2	16.38	4.91	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.38 Tc(MIN.) = 4.91
 TOTAL AREA(ACRES) = 3.1
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 121.00 = 842.00 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 116.01 DOWNSTREAM(FEET) = 112.93
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.5 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 15.28
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 16.38
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 4.96
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 125.00 = 892.00 FEET.

FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<

FLOW PROCESS FROM NODE 148.00 TO NODE 149.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 129.50

DOWNSTREAM ELEVATION(FEET) = 119.80

ELEVATION DIFFERENCE(FEET) = 9.70

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.362

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN T_c CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON T_c = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.75

TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.75

+-----+
| AREA FORCE DRAINED VIA PUMP |
| ADDED AS SUBAREA AT PRESSURE PIPE DISCHARGE POINT |
| |
+-----+

FLOW PROCESS FROM NODE 149.00 TO NODE 149.00 IS CODE = 81

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON T_c = 5-MINUTE.

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.8100

SUBAREA AREA(ACRES) = 0.23 SUBAREA RUNOFF(CFS) = 1.23

TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.97

TC(MIN.) = 2.36

FLOW PROCESS FROM NODE 149.00 TO NODE 590.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 115.80 DOWNSTREAM(FEET) = 114.25

FLOW LENGTH(FEET) = 103.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 9.0 INCH PIPE IS 7.3 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.11

ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.97

PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 2.70
LONGEST FLOWPATH FROM NODE 148.00 TO NODE 590.00 = 198.00 FEET.

FLOW PROCESS FROM NODE 590.00 TO NODE 590.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 2.70
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.37
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.97

FLOW PROCESS FROM NODE 131.00 TO NODE 540.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 53.00
UPSTREAM ELEVATION(FEET) = 124.30
DOWNSTREAM ELEVATION(FEET) = 121.10
ELEVATION DIFFERENCE(FEET) = 3.20
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.087
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.48
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.48

FLOW PROCESS FROM NODE 540.00 TO NODE 132.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 121.10 DOWNSTREAM ELEVATION(FEET) = 117.36
STREET LENGTH(FEET) = 65.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.04
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.20
HALFSTREET FLOOD WIDTH(FEET) = 3.91
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.84
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 2.37
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.21 SUBAREA RUNOFF(CFS) = 1.12
TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.60

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.25
FLOW VELOCITY(FEET/SEC.) = 4.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.94
LONGEST FLOWPATH FROM NODE 131.00 TO NODE 132.00 = 118.00 FEET.

FLOW PROCESS FROM NODE 132.00 TO NODE 590.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	114.36	DOWNSTREAM(FEET) =	114.25
FLOW LENGTH(FEET) =	11.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	9.0 INCH PIPE IS	7.3 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	4.16		
ESTIMATED PIPE DIAMETER(INCH) =	9.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	1.60		
PIPE TRAVEL TIME(MIN.) =	0.04	Tc(MIN.) =	2.41
LONGEST FLOWPATH FROM NODE	131.00 TO NODE	590.00 =	129.00 FEET.

FLOW PROCESS FROM NODE 590.00 TO NODE 590.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM	2 ARE:
TIME OF CONCENTRATION(MIN.) =	2.41
RAINFALL INTENSITY(INCH/HR) =	6.59
TOTAL STREAM AREA(ACRES) =	0.30
PEAK FLOW RATE(CFS) AT CONFLUENCE =	1.60

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.97	2.70	6.587	0.37
2	1.60	2.41	6.587	0.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.37	2.41	6.587
2	3.57	2.70	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.57 Tc(MIN.) = 2.70

TOTAL AREA(ACRES) = 0.7

LONGEST FLOWPATH FROM NODE 148.00 TO NODE 590.00 = 198.00 FEET.

FLOW PROCESS FROM NODE 590.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 114.25 DOWNSTREAM(FEET) = 112.93

FLOW LENGTH(FEET) = 132.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.30

ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.57

PIPE TRAVEL TIME(MIN.) = 0.42 Tc(MIN.) = 3.11

LONGEST FLOWPATH FROM NODE 148.00 TO NODE 125.00 = 330.00 FEET.

FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<

=====

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.57	3.11	6.587	0.67

LONGEST FLOWPATH FROM NODE 148.00 TO NODE 125.00 = 330.00 FEET.

** MEMORY BANK # 2 CONFLUENCE DATA **

STREAM	RUNOFF	Tc	INTENSITY	AREA
--------	--------	----	-----------	------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)	(ACRE)
1	16.38	4.96	6.587	3.07

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 125.00 = 892.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	13.85	3.11	6.587
2	19.95	4.96	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.95 Tc(MIN.) = 4.96
TOTAL AREA(ACRES) = 3.7

FLOW PROCESS FROM NODE 125.00 TO NODE 126.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 112.93 DOWNSTREAM(FEET) = 108.69
FLOW LENGTH(FEET) = 78.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.12
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 19.95
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 5.05
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 126.00 = 970.00 FEET.

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.05
RAINFALL INTENSITY(INCH/HR) = 6.55
TOTAL STREAM AREA(ACRES) = 3.74
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.95

FLOW PROCESS FROM NODE 133.00 TO NODE 550.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 37.00

UPSTREAM ELEVATION(FEET) = 119.66
DOWNSTREAM ELEVATION(FEET) = 117.30
ELEVATION DIFFERENCE(FEET) = 2.36
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.712
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.37
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.37

FLOW PROCESS FROM NODE 550.00 TO NODE 134.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 117.30 DOWNSTREAM ELEVATION(FEET) = 113.12
STREET LENGTH(FEET) = 77.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.80
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.19
HALFSTREET FLOOD WIDTH(FEET) = 3.10
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.74
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.70
STREET FLOW TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 2.06
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.85
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 1.23

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.22 HALFSTREET FLOOD WIDTH(FEET) = 4.51
FLOW VELOCITY(FEET/SEC.) = 3.82 DEPTH*VELOCITY(FT*FT/SEC.) = 0.83
LONGEST FLOWPATH FROM NODE 133.00 TO NODE 134.00 = 114.00 FEET.

FLOW PROCESS FROM NODE 134.00 TO NODE 126.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 110.12 DOWNSTREAM(FEET) = 108.69
FLOW LENGTH(FEET) = 143.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.01
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.23
PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 2.65
LONGEST FLOWPATH FROM NODE 133.00 TO NODE 126.00 = 257.00 FEET.

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 2.65
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.23
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.23

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	19.95	5.05	6.546	3.74
2	1.23	2.65	6.587	0.23

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.70	2.65	6.587
2	21.17	5.05	6.546

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 21.17 Tc(MIN.) = 5.05
TOTAL AREA(ACRES) = 4.0
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 126.00 = 970.00 FEET.

FLOW PROCESS FROM NODE 126.00 TO NODE 127.00 IS CODE = 31

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>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 108.69 DOWNSTREAM(FEET) = 107.84
FLOW LENGTH(FEET) = 20.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.16
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 21.17
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 5.07
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 127.00 = 990.00 FEET.

*****
FLOW PROCESS FROM NODE 127.00 TO NODE 127.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.07
RAINFALL INTENSITY(INCH/HR) = 6.53
TOTAL STREAM AREA(ACRES) = 3.97
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.17

*****
FLOW PROCESS FROM NODE 100.00 TO NODE 600.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 181.00
DOWNSTREAM ELEVATION(FEET) = 172.00
ELEVATION DIFFERENCE(FEET) = 9.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.390
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.275
SUBAREA RUNOFF(CFS) = 0.11
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.11

*****
FLOW PROCESS FROM NODE 600.00 TO NODE 160.00 IS CODE = 51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 172.00 DOWNSTREAM(FEET) = 132.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 333.00 CHANNEL SLOPE = 0.1201
CHANNEL BASE(FEET) = 1.00 "Z" FACTOR = 2.000

```

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.507
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .4500
 S.C.S. CURVE NUMBER (AMC II) = 0
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.29
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.59
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.21
 Tc(MIN.) = 6.60
 SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.35
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.45

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 5.46
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 160.00 = 428.00 FEET.

FLOW PROCESS FROM NODE 160.00 TO NODE 128.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 129.00 DOWNSTREAM(FEET) = 125.76
 FLOW LENGTH(FEET) = 122.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.0 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.52
 ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 0.45
 PIPE TRAVEL TIME(MIN.) = 0.45 Tc(MIN.) = 7.05
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 128.00 = 550.00 FEET.

FLOW PROCESS FROM NODE 128.00 TO NODE 130.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 125.76 DOWNSTREAM ELEVATION(FEET) = 117.50
 STREET LENGTH(FEET) = 156.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.65
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.24
 HALFSTREET FLOOD WIDTH(FEET) = 5.47
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.96
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.93
 STREET FLOW TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 7.70
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.984
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100
 S.C.S. CURVE NUMBER (AMC II) = 0
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.727
 SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 2.42
 TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 2.83

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.25
 FLOW VELOCITY(FEET/SEC.) = 4.39 DEPTH*VELOCITY(FT*FT/SEC.) = 1.19
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 130.00 = 706.00 FEET.

FLOW PROCESS FROM NODE 130.00 TO NODE 127.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 108.06 DOWNSTREAM(FEET) = 107.84
 FLOW LENGTH(FEET) = 4.50 MANNING'S N = 0.013
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.1 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.94
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 2.83
 PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 7.71
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 127.00 = 710.50 FEET.

FLOW PROCESS FROM NODE 127.00 TO NODE 127.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 7.71
 RAINFALL INTENSITY(INCH/HR) = 4.98
 TOTAL STREAM AREA(ACRES) = 0.78
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.83

FLOW PROCESS FROM NODE 103.00 TO NODE 136.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 150.62

DOWNSTREAM ELEVATION(FEET) = 145.21

ELEVATION DIFFERENCE(FEET) = 5.41

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.849

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.27

TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.27

FLOW PROCESS FROM NODE 136.00 TO NODE 137.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====

UPSTREAM ELEVATION(FEET) = 145.21 DOWNSTREAM ELEVATION(FEET) = 117.57

STREET LENGTH(FEET) = 543.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.25

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.22

HALFSTREET FLOOD WIDTH(FEET) = 4.65

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.73

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.82

STREET FLOW TRAVEL TIME(MIN.) = 2.43 Tc(MIN.) = 5.28

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.361

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.810

SUBAREA AREA(ACRES) = 0.38 SUBAREA RUNOFF(CFS) = 1.96

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 2.22

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.44

FLOW VELOCITY(FEET/SEC.) = 4.16 DEPTH*VELOCITY(FT*FT/SEC.) = 1.06

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 137.00 = 638.00 FEET.

FLOW PROCESS FROM NODE 137.00 TO NODE 127.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 108.72 DOWNSTREAM(FEET) = 107.84

FLOW LENGTH(FEET) = 18.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 8.51

ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 2.22

PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 5.31

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 127.00 = 656.00 FEET.

FLOW PROCESS FROM NODE 127.00 TO NODE 127.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:

TIME OF CONCENTRATION(MIN.) = 5.31

RAINFALL INTENSITY(INCH/HR) = 6.33

TOTAL STREAM AREA(ACRES) = 0.43

PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.22

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	21.17	5.07	6.526	3.97
2	2.83	7.71	4.980	0.78
3	2.22	5.31	6.334	0.43

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	25.15	5.07	6.526
2	24.71	5.31	6.334
3	20.73	7.71	4.980

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 25.15 Tc(MIN.) = 5.07

TOTAL AREA(ACRES) = 5.2

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 127.00 = 990.00 FEET.

FLOW PROCESS FROM NODE 127.00 TO NODE 140.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 107.84 DOWNSTREAM(FEET) = 106.00

FLOW LENGTH(FEET) = 46.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 14.31

ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 25.15

PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 5.13

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 140.00 = 1036.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

FLOW PROCESS FROM NODE 130.00 TO NODE 141.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 40.00

UPSTREAM ELEVATION(FEET) = 117.50

DOWNSTREAM ELEVATION(FEET) = 114.93

ELEVATION DIFFERENCE(FEET) = 2.57

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.776

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.16

TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.16

FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<

UPSTREAM ELEVATION(FEET) = 114.93 DOWNSTREAM ELEVATION(FEET) = 110.22
STREET LENGTH(FEET) = 126.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.45
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.16
HALFSTREET FLOOD WIDTH(FEET) = 1.50
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.65
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.57
STREET FLOW TRAVEL TIME(MIN.) = 0.58 Tc(MIN.) = 2.35
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.59
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.75

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.20 HALFSTREET FLOOD WIDTH(FEET) = 3.54
FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.60
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 142.00 = 166.00 FEET.

FLOW PROCESS FROM NODE 142.00 TO NODE 142.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 2.35
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.14
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.75

FLOW PROCESS FROM NODE 144.00 TO NODE 142.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00
UPSTREAM ELEVATION(FEET) = 115.00
DOWNSTREAM ELEVATION(FEET) = 110.22
ELEVATION DIFFERENCE(FEET) = 4.78
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.160
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.454
SUBAREA RUNOFF(CFS) = 0.17
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.17

*****
FLOW PROCESS FROM NODE 142.00 TO NODE 142.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.16
RAINFALL INTENSITY(INCH/HR) = 6.45
TOTAL STREAM AREA(ACRES) = 0.06
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
    1         0.75      2.35      6.587         0.14
    2         0.17      5.16      6.454         0.06

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
    1         0.83      2.35      6.587
    2         0.91      5.16      6.454

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 0.91 Tc(MIN.) = 5.16
TOTAL AREA(ACRES) = 0.2
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 142.00 = 166.00 FEET.

*****
FLOW PROCESS FROM NODE 142.00 TO NODE 139.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

```

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 106.70 DOWNSTREAM(FEET) = 106.40
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.04
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.91
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 5.26
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 139.00 = 191.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 139.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.26
RAINFALL INTENSITY(INCH/HR) = 6.37
TOTAL STREAM AREA(ACRES) = 0.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.91

FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 117.57
DOWNSTREAM ELEVATION(FEET) = 114.93
ELEVATION DIFFERENCE(FEET) = 2.64
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.136
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.27

FLOW PROCESS FROM NODE 138.00 TO NODE 139.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 114.93 DOWNSTREAM ELEVATION(FEET) = 110.22
STREET LENGTH(FEET) = 91.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.40
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FT) = 0.16
HALFSTREET FLOOD WIDTH(FT) = 1.50
AVERAGE FLOW VELOCITY(FT/SEC.) = 4.29
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.67
STREET FLOW TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 3.49
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.53

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FT) = 0.16 HALFSTREET FLOOD WIDTH(FT) = 1.50
FLOW VELOCITY(FT/SEC.) = 4.29 DEPTH*VELOCITY(FT*FT/SEC.) = 0.67
LONGEST FLOWPATH FROM NODE 137.00 TO NODE 139.00 = 171.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 139.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.49
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.53

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.91	5.26	6.372	0.20
2	0.53	3.49	6.587	0.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.41	3.49	6.587
2	1.42	5.26	6.372

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 1.42 Tc(MIN.) = 5.26
TOTAL AREA(ACRES) = 0.3
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 139.00 = 191.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 140.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 106.40 DOWNSTREAM(FEET) = 106.00
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.11
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.42
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.43
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 140.00 = 231.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 11

>>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.42	5.43	6.249	0.30

LONGEST FLOWPATH FROM NODE 130.00 TO NODE 140.00 = 231.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	25.15	5.13	6.482	5.18

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 140.00 = 1036.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
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1	26.49	5.13	6.482
2	25.66	5.43	6.249

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.49 Tc(MIN.) = 5.13
 TOTAL AREA(ACRES) = 5.5

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

FLOW PROCESS FROM NODE 146.00 TO NODE 147.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 116.27

DOWNSTREAM ELEVATION(FEET) = 110.79

ELEVATION DIFFERENCE(FEET) = 5.48

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.837

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.69

TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.69

FLOW PROCESS FROM NODE 147.00 TO NODE 140.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 107.79 DOWNSTREAM(FEET) = 106.00

FLOW LENGTH(FEET) = 3.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 15.91

ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.69

PIPE TRAVEL TIME(MIN.) = 0.00 Tc(MIN.) = 2.84

LONGEST FLOWPATH FROM NODE 146.00 TO NODE 140.00 = 98.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<
=====

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.69	2.84	6.587	0.13

LONGEST FLOWPATH FROM NODE 146.00 TO NODE 140.00 = 98.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	26.49	5.13	6.482	5.48

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 140.00 = 1036.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	15.37	2.84	6.587
2	27.17	5.13	6.482

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 27.17 Tc(MIN.) = 5.13
TOTAL AREA(ACRES) = 5.6

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.482
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7951
SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 1.00
TOTAL AREA(ACRES) = 5.8 TOTAL RUNOFF(CFS) = 29.89
TC(MIN.) = 5.13

FLOW PROCESS FROM NODE 140.00 TO NODE 300.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 94.20 DOWNSTREAM(FEET) = 92.00
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.30
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 29.89
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.29
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 300.00 = 1146.00 FEET.

FLOW PROCESS FROM NODE 300.00 TO NODE 700.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 92.00 DOWNSTREAM(FEET) = 84.00
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 32.51
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 29.89
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 5.30
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 700.00 = 1171.00 FEET.

+-----+
| END FLOWS TO POC-A |
| |
+-----+

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END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 5.8 TC(MIN.) = 5.30

PEAK FLOW RATE(CFS) = 29.89

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END OF RATIONAL METHOD ANALYSIS



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
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***** DESCRIPTION OF STUDY *****
* PIRAEUS STREET, ENCINITAS *
* POST-DEVELOPMENT MITIGATED ANALYSIS *
* *

FILE NAME: 3733PSTM.DAT
TIME/DATE OF STUDY: 15:24 09/08/2022

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 2.500
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	12.0	1.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

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BEGIN FLOWS TO POC-B

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

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*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 174.70

DOWNSTREAM ELEVATION(FEET) = 142.09

ELEVATION DIFFERENCE(FEET) = 32.61

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.431

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.245

SUBAREA RUNOFF(CFS) = 0.67

TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.67

FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 142.09 DOWNSTREAM(FEET) = 80.34

CHANNEL LENGTH THRU SUBAREA(FEET) = 492.00 CHANNEL SLOPE = 0.1255

CHANNEL BASE(FEET) = 3.50 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 28.50

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.099

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.82

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.09

AVERAGE FLOW DEPTH(FEET) = 0.12 TRAVEL TIME(MIN.) = 2.01

Tc(MIN.) = 7.44

SUBAREA AREA(ACRES) = 0.99 SUBAREA RUNOFF(CFS) = 2.27

AREA-AVERAGE RUNOFF COEFFICIENT = 0.450

TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 2.82

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 4.76

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 592.00 FEET.

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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TOTAL NUMBER OF STREAMS = 5
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 7.44
RAINFALL INTENSITY(INCH/HR) = 5.10
TOTAL STREAM AREA(ACRES) = 1.23
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.82

FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 108.00
DOWNSTREAM ELEVATION(FEET) = 95.20
ELEVATION DIFFERENCE(FEET) = 12.80
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.431
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.245
SUBAREA RUNOFF(CFS) = 0.14
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.14

FLOW PROCESS FROM NODE 204.00 TO NODE 202.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 95.20 DOWNSTREAM(FEET) = 80.34
CHANNEL LENGTH THRU SUBAREA(FEET) = 790.00 CHANNEL SLOPE = 0.0188
CHANNEL BASE(FEET) = 1.50 "Z" FACTOR = 12.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 0.50
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.328
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.72
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.47
AVERAGE FLOW DEPTH(FEET) = 0.15 TRAVEL TIME(MIN.) = 8.98
Tc(MIN.) = 14.41
SUBAREA AREA(ACRES) = 0.75 SUBAREA RUNOFF(CFS) = 1.12
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 1.20

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.19 FLOW VELOCITY(FEET/SEC.) = 1.62

LONGEST FLOWPATH FROM NODE 203.00 TO NODE 202.00 = 890.00 FEET.

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 5

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 14.41

RAINFALL INTENSITY(INCH/HR) = 3.33

TOTAL STREAM AREA(ACRES) = 0.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.20

FLOW PROCESS FROM NODE 153.00 TO NODE 153.00 IS CODE = 81

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.328

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.5036

SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.38

TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 1.58

TC(MIN.) = 14.41

FLOW PROCESS FROM NODE 153.00 TO NODE 500.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 93.00 DOWNSTREAM(FEET) = 90.52

FLOW LENGTH(FEET) = 29.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 6.0 INCH PIPE IS 4.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 9.29

ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.58

PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 14.46

LONGEST FLOWPATH FROM NODE 0.00 TO NODE 500.00 = 29.00 FEET.

FLOW PROCESS FROM NODE 500.00 TO NODE 202.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

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UPSTREAM ELEVATION(FEET) = 90.52 DOWNSTREAM ELEVATION(FEET) = 80.34
STREET LENGTH(FEET) = 333.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.59
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.25
HALFSTREET FLOOD WIDTH(FEET) = 6.21
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.15
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.79
STREET FLOW TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 16.23
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.083

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.507
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.02
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 1.58

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.21
FLOW VELOCITY(FEET/SEC.) = 3.12 DEPTH*VELOCITY(FT*FT/SEC.) = 0.78
LONGEST FLOWPATH FROM NODE 0.00 TO NODE 202.00 = 362.00 FEET.

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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TOTAL NUMBER OF STREAMS = 5
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 16.23
RAINFALL INTENSITY(INCH/HR) = 3.08
TOTAL STREAM AREA(ACRES) = 0.95
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.58

FLOW PROCESS FROM NODE 154.00 TO NODE 154.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.083
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5458
SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.35
TOTAL AREA(ACRES) = 1.1 TOTAL RUNOFF(CFS) = 1.83
TC(MIN.) = 16.23
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FLOW PROCESS FROM NODE 154.00 TO NODE 202.00 IS CODE = 51

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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
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ELEVATION DATA: UPSTREAM(FEET) = 90.00 DOWNSTREAM(FEET) = 80.34
CHANNEL LENGTH THRU SUBAREA(FEET) = 114.00 CHANNEL SLOPE = 0.0847
CHANNEL BASE(FEET) = 2.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.048
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.85
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.57
AVERAGE FLOW DEPTH(FEET) = 0.12 TRAVEL TIME(MIN.) = 0.29
Tc(MIN.) = 16.52
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.02
AREA-AVERAGE RUNOFF COEFFICIENT = 0.548
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 1.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 6.54
LONGEST FLOWPATH FROM NODE 0.00 TO NODE 202.00 = 114.00 FEET.
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+-----+
| ADD SUBAREA B-7 AT NODE 510 |
|                               |
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FLOW PROCESS FROM NODE 510.00 TO NODE 510.00 IS CODE = 81

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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.048
*USER SPECIFIED(SUBAREA):
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USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5378
SUBAREA AREA(ACRES) = 0.13 SUBAREA RUNOFF(CFS) = 0.18
TOTAL AREA(ACRES) = 1.2 TOTAL RUNOFF(CFS) = 2.02
TC(MIN.) = 16.52

FLOW PROCESS FROM NODE 510.00 TO NODE 143.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 64.00
UPSTREAM ELEVATION(FEET) = 150.50
DOWNSTREAM ELEVATION(FEET) = 127.00
ELEVATION DIFFERENCE(FEET) = 23.50
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.345
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.12
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.12

FLOW PROCESS FROM NODE 143.00 TO NODE 145.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 127.00 DOWNSTREAM(FEET) = 111.34
CHANNEL LENGTH THRU SUBAREA(FEET) = 180.00 CHANNEL SLOPE = 0.0870
CHANNEL BASE(FEET) = 2.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.354

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.27
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.18
AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 0.94
Tc(MIN.) = 5.29
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.31
AREA-AVERAGE RUNOFF COEFFICIENT = 0.666
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.42

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 3.98

LONGEST FLOWPATH FROM NODE 510.00 TO NODE 145.00 = 244.00 FEET.

FLOW PROCESS FROM NODE 145.00 TO NODE 202.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

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UPSTREAM ELEVATION(FEET) = 111.34 DOWNSTREAM ELEVATION(FEET) = 80.34

STREET LENGTH(FEET) = 1213.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.44

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.17

HALFSTREET FLOOD WIDTH(FEET) = 2.13

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.68

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.45

STREET FLOW TRAVEL TIME(MIN.) = 7.55 Tc(MIN.) = 12.84

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.585

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.679

SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.03

TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.42

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.16 HALFSTREET FLOOD WIDTH(FEET) = 1.50

FLOW VELOCITY(FEET/SEC.) = 3.02 DEPTH*VELOCITY(FT*FT/SEC.) = 0.47

LONGEST FLOWPATH FROM NODE 510.00 TO NODE 202.00 = 1457.00 FEET.

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

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TOTAL NUMBER OF STREAMS = 5

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 5 ARE:

TIME OF CONCENTRATION(MIN.) = 12.84

RAINFALL INTENSITY(INCH/HR) = 3.58
TOTAL STREAM AREA(ACRES) = 0.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.42

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.82	7.44	5.099	1.23
2	1.20	14.41	3.328	0.80
3	1.58	16.23	3.083	0.95
5	0.42	12.84	3.585	0.11

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 5 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	0.00	0.00	6.587
2	4.41	7.44	5.099
3	4.72	12.84	3.585
4	4.83	14.41	3.328
5	4.76	16.23	3.083

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.83 Tc(MIN.) = 14.41
TOTAL AREA(ACRES) = 3.1
LONGEST FLOWPATH FROM NODE 510.00 TO NODE 202.00 = 1457.00 FEET.

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+-----+
| END FLOWS TO POC-B |
|                     |
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+-----+
| BEGIN FLOWS TO POC-A |
|                     |
+-----+
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FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
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*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00

UPSTREAM ELEVATION(FEET) = 181.00
DOWNSTREAM ELEVATION(FEET) = 172.00
ELEVATION DIFFERENCE(FEET) = 9.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.625
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.16

FLOW PROCESS FROM NODE 101.00 TO NODE 151.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 156.53 DOWNSTREAM(FEET) = 156.00
FLOW LENGTH(FEET) = 10.50 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 6.000
DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.39
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.16
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 1.67
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 151.00 = 55.50 FEET.

FLOW PROCESS FROM NODE 151.00 TO NODE 102.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 156.00 DOWNSTREAM ELEVATION(FEET) = 138.54
STREET LENGTH(FEET) = 321.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.35
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.26
HALFSTREET FLOOD WIDTH(FEET) = 6.58
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.26

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.10
 STREET FLOW TRAVEL TIME(MIN.) = 1.26 Tc(MIN.) = 2.92
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100
 S.C.S. CURVE NUMBER (AMC II) = 0
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
 SUBAREA AREA(ACRES) = 0.82 SUBAREA RUNOFF(CFS) = 4.37
 TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 4.54

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.96
 FLOW VELOCITY(FEET/SEC.) = 4.93 DEPTH*VELOCITY(FT*FT/SEC.) = 1.50
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 376.50 FEET.

 FLOW PROCESS FROM NODE 102.00 TO NODE 114.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
 ELEVATION DATA: UPSTREAM(FEET) = 128.34 DOWNSTREAM(FEET) = 128.12
 FLOW LENGTH(FEET) = 4.50 MANNING'S N = 0.013
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.19
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 4.54
 PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 2.93
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 114.00 = 381.00 FEET.

 FLOW PROCESS FROM NODE 114.00 TO NODE 114.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100
 S.C.S. CURVE NUMBER (AMC II) = 0
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
 UPSTREAM ELEVATION(FEET) = 150.62
 DOWNSTREAM ELEVATION(FEET) = 146.63
 ELEVATION DIFFERENCE(FEET) = 3.99
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.086

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
 THE MAXIMUM OVERLAND FLOW LENGTH = 91.00
 (Reference: Table 3-1B of Hydrology Manual)
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) = 0.69
 TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.69

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 62

 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<
 =====

UPSTREAM ELEVATION(FEET) = 146.63 DOWNSTREAM ELEVATION(FEET) = 140.51
 STREET LENGTH(FEET) = 97.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.17
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.21
 HALFSTREET FLOOD WIDTH(FEET) = 4.13
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.06
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
 STREET FLOW TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 3.48
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100
 S.C.S. CURVE NUMBER (AMC II) = 0
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
 SUBAREA AREA(ACRES) = 0.18 SUBAREA RUNOFF(CFS) = 0.96
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.65

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.17
 FLOW VELOCITY(FEET/SEC.) = 4.29 DEPTH*VELOCITY(FT*FT/SEC.) = 0.98
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 105.00 = 192.00 FEET.

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 137.51 DOWNSTREAM(FEET) = 133.85
FLOW LENGTH(FEET) = 82.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.67
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.65
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 3.66
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 106.00 = 274.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 3.66
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.65

FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 146.18
DOWNSTREAM ELEVATION(FEET) = 140.74
ELEVATION DIFFERENCE(FEET) = 5.44
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.844
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.96

FLOW PROCESS FROM NODE 108.00 TO NODE 106.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 140.74 DOWNSTREAM ELEVATION(FEET) = 136.85
STREET LENGTH(FEET) = 70.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.36
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.22
HALFSTREET FLOOD WIDTH(FEET) = 4.80
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.90
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.87
STREET FLOW TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 3.14
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.15 SUBAREA RUNOFF(CFS) = 0.80
TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.76

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 5.62
FLOW VELOCITY(FEET/SEC.) = 4.06 DEPTH*VELOCITY(FT*FT/SEC.) = 0.97
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 106.00 = 165.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.14
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.33
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.76

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
------------------	-----------------	--------------	--------------------------	----------------

1	1.65	3.66	6.587	0.31
2	1.76	3.14	6.587	0.33

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.18	3.14	6.587
2	3.41	3.66	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.41 Tc(MIN.) = 3.66

TOTAL AREA(ACRES) = 0.6

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 106.00 = 274.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 109.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 133.85 DOWNSTREAM(FEET) = 131.86

FLOW LENGTH(FEET) = 199.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.03

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.41

PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 4.32

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 109.00 = 473.00 FEET.

FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 131.86 DOWNSTREAM(FEET) = 129.61

FLOW LENGTH(FEET) = 78.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.78

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.41

PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 4.49

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 110.00 = 551.00 FEET.

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.49
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.64
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.41
```

FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 142.09
DOWNSTREAM ELEVATION(FEET) = 136.65
ELEVATION DIFFERENCE(FEET) = 5.44
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.844
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.96
```

FLOW PROCESS FROM NODE 112.00 TO NODE 113.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

```
=====
UPSTREAM ELEVATION(FEET) = 136.65 DOWNSTREAM ELEVATION(FEET) = 134.29
STREET LENGTH(FEET) = 41.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00
```

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.28
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.22
HALFSTREET FLOOD WIDTH(FEET) = 4.58

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.91
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
 STREET FLOW TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 3.02
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100
 S.C.S. CURVE NUMBER (AMC II) = 0
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
 SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 0.64
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.60

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.25
 FLOW VELOCITY(FEET/SEC.) = 4.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.94
 LONGEST FLOWPATH FROM NODE 111.00 TO NODE 113.00 = 136.00 FEET.

FLOW PROCESS FROM NODE 113.00 TO NODE 110.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 131.29 DOWNSTREAM(FEET) = 129.61
 FLOW LENGTH(FEET) = 168.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 7.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.16
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 1.60
 PIPE TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 3.69
 LONGEST FLOWPATH FROM NODE 111.00 TO NODE 110.00 = 304.00 FEET.

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 3.69
 RAINFALL INTENSITY(INCH/HR) = 6.59
 TOTAL STREAM AREA(ACRES) = 0.30
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.60

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.41	4.49	6.587	0.64
2	1.60	3.69	6.587	0.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.02	3.69	6.587
2	5.02	4.49	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.02 Tc(MIN.) = 4.49
TOTAL AREA(ACRES) = 0.9
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 110.00 = 551.00 FEET.

FLOW PROCESS FROM NODE 110.00 TO NODE 114.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 129.61 DOWNSTREAM(FEET) = 128.12
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.55
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.02
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 4.59
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 114.00 = 601.00 FEET.

FLOW PROCESS FROM NODE 114.00 TO NODE 114.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	5.02	4.59	6.587	0.94

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 114.00 = 601.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.54	2.93	6.587	0.85

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 114.00 = 381.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM	RUNOFF	Tc	INTENSITY
--------	--------	----	-----------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)
1	7.74	2.93	6.587
2	9.55	4.59	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.55 Tc(MIN.) = 4.59
TOTAL AREA(ACRES) = 1.8

FLOW PROCESS FROM NODE 114.00 TO NODE 114.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<
=====

FLOW PROCESS FROM NODE 114.00 TO NODE 115.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 128.12 DOWNSTREAM(FEET) = 127.37
FLOW LENGTH(FEET) = 24.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.19
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.55
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 4.63
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 115.00 = 625.00 FEET.

FLOW PROCESS FROM NODE 115.00 TO NODE 115.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.63
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 1.79
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.55

FLOW PROCESS FROM NODE 116.00 TO NODE 530.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 30.00

UPSTREAM ELEVATION(FEET) = 138.00
DOWNSTREAM ELEVATION(FEET) = 136.30
ELEVATION DIFFERENCE(FEET) = 1.70
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.604
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.32
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.32

FLOW PROCESS FROM NODE 530.00 TO NODE 117.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	136.30	DOWNSTREAM ELEVATION(FEET) =	131.74
STREET LENGTH(FEET) =	78.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	12.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.80
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.19
HALFSTREET FLOOD WIDTH(FEET) = 3.02
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.82
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.71
STREET FLOW TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 1.94
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.18 SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 1.28

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.22 HALFSTREET FLOOD WIDTH(FEET) = 4.51
FLOW VELOCITY(FEET/SEC.) = 3.99 DEPTH*VELOCITY(FT*FT/SEC.) = 0.86
LONGEST FLOWPATH FROM NODE 116.00 TO NODE 117.00 = 108.00 FEET.

FLOW PROCESS FROM NODE 117.00 TO NODE 115.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 128.74 DOWNSTREAM(FEET) = 127.37
FLOW LENGTH(FEET) = 137.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.05
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.28
PIPE TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 2.51
LONGEST FLOWPATH FROM NODE 116.00 TO NODE 115.00 = 245.00 FEET.

FLOW PROCESS FROM NODE 115.00 TO NODE 155.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 2.51
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.24
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.28

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	9.55	4.63	6.587	1.79
2	1.28	2.51	6.587	0.24

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	6.46	2.51	6.587
2	10.83	4.63	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 10.83 Tc(MIN.) = 4.63
TOTAL AREA(ACRES) = 2.0
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 155.00 = 625.00 FEET.

FLOW PROCESS FROM NODE 115.00 TO NODE 118.00 IS CODE = 31

```

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 127.37 DOWNSTREAM(FEET) = 124.46
FLOW LENGTH(FEET) = 78.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 11.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.20
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.83
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 4.74
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 118.00 = 703.00 FEET.

*****
FLOW PROCESS FROM NODE 118.00 TO NODE 118.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.74
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 2.03
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.83

*****
FLOW PROCESS FROM NODE 119.00 TO NODE 120.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 93.00
UPSTREAM ELEVATION(FEET) = 133.92
DOWNSTREAM ELEVATION(FEET) = 128.64
ELEVATION DIFFERENCE(FEET) = 5.28
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.822
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.96

*****
FLOW PROCESS FROM NODE 120.00 TO NODE 118.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 125.64 DOWNSTREAM(FEET) = 124.46
FLOW LENGTH(FEET) = 118.00 MANNING'S N = 0.013

```

DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.82
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.96
PIPE TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 3.34
LONGEST FLOWPATH FROM NODE 119.00 TO NODE 118.00 = 211.00 FEET.

FLOW PROCESS FROM NODE 118.00 TO NODE 118.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.34
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.18
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.96

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	10.83	4.74	6.587	2.03
2	0.96	3.34	6.587	0.18

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.79	3.34	6.587
2	11.79	4.74	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.79 Tc(MIN.) = 4.74
TOTAL AREA(ACRES) = 2.2
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 118.00 = 703.00 FEET.

FLOW PROCESS FROM NODE 118.00 TO NODE 121.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 124.46 DOWNSTREAM(FEET) = 116.01
FLOW LENGTH(FEET) = 139.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.92

ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.79
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 4.91
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 121.00 = 842.00 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 121.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.91
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 2.21
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.79

FLOW PROCESS FROM NODE 156.00 TO NODE 123.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 143.00
DOWNSTREAM ELEVATION(FEET) = 138.63
ELEVATION DIFFERENCE(FEET) = 4.37
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.027
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
 THE MAXIMUM OVERLAND FLOW LENGTH = 93.00
 (Reference: Table 3-1B of Hydrology Manual)
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.91
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.91

FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 138.63 DOWNSTREAM ELEVATION(FEET) = 125.78
STREET LENGTH(FEET) = 245.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.75
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(Feet) = 0.27
HALFSTREET FLOOD WIDTH(Feet) = 7.18
AVERAGE FLOW VELOCITY(Feet/Sec.) = 4.34
PRODUCT OF DEPTH&VELOCITY(Feet*Feet/Sec.) = 1.17
STREET FLOW TRAVEL TIME(Min.) = 0.94 Tc(Min.) = 3.97
100 YEAR RAINFALL INTENSITY(Inch/Hour) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.69 SUBAREA RUNOFF(CFS) = 3.68
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 4.59

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(Feet) = 0.31 HALFSTREET FLOOD WIDTH(Feet) = 9.03
FLOW VELOCITY(Feet/Sec.) = 4.91 DEPTH*VELOCITY(Feet*Feet/Sec.) = 1.51
LONGEST FLOWPATH FROM NODE 156.00 TO NODE 124.00 = 340.00 FEET.

FLOW PROCESS FROM NODE 124.00 TO NODE 121.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 116.23 DOWNSTREAM(Feet) = 116.01
FLOW LENGTH(Feet) = 4.50 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.7 INCHES
PIPE-FLOW VELOCITY(Feet/Sec.) = 10.21
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.59
PIPE TRAVEL TIME(Min.) = 0.01 Tc(Min.) = 3.98
LONGEST FLOWPATH FROM NODE 156.00 TO NODE 121.00 = 344.50 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 121.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 3.98
 RAINFALL INTENSITY(INCH/HR) = 6.59
 TOTAL STREAM AREA(ACRES) = 0.86
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.59

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	11.79	4.91	6.587	2.21
2	4.59	3.98	6.587	0.86

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	16.38	3.98	6.587
2	16.38	4.91	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.38 Tc(MIN.) = 4.91
 TOTAL AREA(ACRES) = 3.1
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 121.00 = 842.00 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 125.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 116.01 DOWNSTREAM(FEET) = 112.93

FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 15.28

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 16.38

PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 4.96

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 125.00 = 892.00 FEET.

FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 10

>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

FLOW PROCESS FROM NODE 148.00 TO NODE 149.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 129.50

DOWNSTREAM ELEVATION(FEET) = 119.80

ELEVATION DIFFERENCE(FEET) = 9.70

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.362

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN T_c CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON T_c = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.75

TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.75

+-----+
| AREA FORCE DRAINED VIA PUMP |

| ADDED AS SUBAREA AT PRESSURE PIPE DISCHARGE POINT |

+-----+

FLOW PROCESS FROM NODE 149.00 TO NODE 149.00 IS CODE = 81

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON T_c = 5-MINUTE.

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.8100

SUBAREA AREA(ACRES) = 0.23 SUBAREA RUNOFF(CFS) = 1.23

TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.97

TC(MIN.) = 2.36

FLOW PROCESS FROM NODE 149.00 TO NODE 590.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 115.80 DOWNSTREAM(FEET) = 114.25

FLOW LENGTH(FEET) = 103.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 9.0 INCH PIPE IS 7.3 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.11

ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.97

PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 2.70
LONGEST FLOWPATH FROM NODE 148.00 TO NODE 590.00 = 198.00 FEET.

FLOW PROCESS FROM NODE 590.00 TO NODE 590.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 2.70
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.37
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.97

FLOW PROCESS FROM NODE 131.00 TO NODE 540.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 53.00
UPSTREAM ELEVATION(FEET) = 124.30
DOWNSTREAM ELEVATION(FEET) = 121.10
ELEVATION DIFFERENCE(FEET) = 3.20
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.087
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.48
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.48

FLOW PROCESS FROM NODE 540.00 TO NODE 132.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 121.10 DOWNSTREAM ELEVATION(FEET) = 117.36
STREET LENGTH(FEET) = 65.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.04
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.20
HALFSTREET FLOOD WIDTH(FEET) = 3.91
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.84
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 2.37
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.21 SUBAREA RUNOFF(CFS) = 1.12
TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.60

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.25
FLOW VELOCITY(FEET/SEC.) = 4.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.94
LONGEST FLOWPATH FROM NODE 131.00 TO NODE 132.00 = 118.00 FEET.

FLOW PROCESS FROM NODE 132.00 TO NODE 590.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	114.36	DOWNSTREAM(FEET) =	114.25
FLOW LENGTH(FEET) =	11.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	9.0 INCH PIPE IS	7.3 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	4.16		
ESTIMATED PIPE DIAMETER(INCH) =	9.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	1.60		
PIPE TRAVEL TIME(MIN.) =	0.04	Tc(MIN.) =	2.41
LONGEST FLOWPATH FROM NODE	131.00 TO NODE	590.00 =	129.00 FEET.

FLOW PROCESS FROM NODE 590.00 TO NODE 590.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM	2 ARE:
TIME OF CONCENTRATION(MIN.) =	2.41
RAINFALL INTENSITY(INCH/HR) =	6.59
TOTAL STREAM AREA(ACRES) =	0.30
PEAK FLOW RATE(CFS) AT CONFLUENCE =	1.60

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.97	2.70	6.587	0.37
2	1.60	2.41	6.587	0.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.37	2.41	6.587
2	3.57	2.70	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.57 Tc(MIN.) = 2.70

TOTAL AREA(ACRES) = 0.7

LONGEST FLOWPATH FROM NODE 148.00 TO NODE 590.00 = 198.00 FEET.

FLOW PROCESS FROM NODE 590.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 114.25 DOWNSTREAM(Feet) = 112.93

FLOW LENGTH(Feet) = 132.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.1 INCHES

PIPE-FLOW VELOCITY(Feet/Sec.) = 5.30

ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.57

PIPE TRAVEL TIME(MIN.) = 0.42 Tc(MIN.) = 3.11

LONGEST FLOWPATH FROM NODE 148.00 TO NODE 125.00 = 330.00 FEET.

FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<

=====

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.57	3.11	6.587	0.67

LONGEST FLOWPATH FROM NODE 148.00 TO NODE 125.00 = 330.00 FEET.

** MEMORY BANK # 2 CONFLUENCE DATA **

STREAM	RUNOFF	Tc	INTENSITY	AREA
--------	--------	----	-----------	------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)	(ACRE)
1	16.38	4.96	6.587	3.07

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 125.00 = 892.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	13.85	3.11	6.587
2	19.95	4.96	6.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.95 Tc(MIN.) = 4.96
TOTAL AREA(ACRES) = 3.7

FLOW PROCESS FROM NODE 125.00 TO NODE 126.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 112.93 DOWNSTREAM(FEET) = 108.69
FLOW LENGTH(FEET) = 78.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.12
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 19.95
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 5.05
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 126.00 = 970.00 FEET.

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.05
RAINFALL INTENSITY(INCH/HR) = 6.55
TOTAL STREAM AREA(ACRES) = 3.74
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.95

FLOW PROCESS FROM NODE 133.00 TO NODE 550.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 37.00

UPSTREAM ELEVATION(FEET) = 119.66
DOWNSTREAM ELEVATION(FEET) = 117.30
ELEVATION DIFFERENCE(FEET) = 2.36
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.712
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.37
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.37

FLOW PROCESS FROM NODE 550.00 TO NODE 134.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	117.30	DOWNSTREAM ELEVATION(FEET) =	113.12
STREET LENGTH(FEET) =	77.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	12.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.80
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.19
HALFSTREET FLOOD WIDTH(FEET) = 3.10
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.74
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.70
STREET FLOW TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 2.06
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.85
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 1.23

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.22 HALFSTREET FLOOD WIDTH(FEET) = 4.51
FLOW VELOCITY(FEET/SEC.) = 3.82 DEPTH*VELOCITY(FT*FT/SEC.) = 0.83
LONGEST FLOWPATH FROM NODE 133.00 TO NODE 134.00 = 114.00 FEET.

FLOW PROCESS FROM NODE 134.00 TO NODE 126.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 110.12 DOWNSTREAM(FEET) = 108.69
FLOW LENGTH(FEET) = 143.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.01
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.23
PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 2.65
LONGEST FLOWPATH FROM NODE 133.00 TO NODE 126.00 = 257.00 FEET.

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 2.65
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.23
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.23

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	19.95	5.05	6.546	3.74
2	1.23	2.65	6.587	0.23

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.70	2.65	6.587
2	21.17	5.05	6.546

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 21.17 Tc(MIN.) = 5.05
TOTAL AREA(ACRES) = 4.0
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 126.00 = 970.00 FEET.

FLOW PROCESS FROM NODE 126.00 TO NODE 127.00 IS CODE = 31

```

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 108.69 DOWNSTREAM(FEET) = 107.84
FLOW LENGTH(FEET) = 20.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.16
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 21.17
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 5.07
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 127.00 = 990.00 FEET.

*****
FLOW PROCESS FROM NODE 127.00 TO NODE 127.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.07
RAINFALL INTENSITY(INCH/HR) = 6.53
TOTAL STREAM AREA(ACRES) = 3.97
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.17

*****
FLOW PROCESS FROM NODE 100.00 TO NODE 600.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 181.00
DOWNSTREAM ELEVATION(FEET) = 172.00
ELEVATION DIFFERENCE(FEET) = 9.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.390
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.275
SUBAREA RUNOFF(CFS) = 0.11
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.11

*****
FLOW PROCESS FROM NODE 600.00 TO NODE 160.00 IS CODE = 51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 172.00 DOWNSTREAM(FEET) = 132.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 333.00 CHANNEL SLOPE = 0.1201
CHANNEL BASE(FEET) = 1.00 "Z" FACTOR = 2.000

```

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.507
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .4500
 S.C.S. CURVE NUMBER (AMC II) = 0
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.29
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.59
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.21
 Tc(MIN.) = 6.60
 SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.35
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.45

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 5.46
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 160.00 = 428.00 FEET.

FLOW PROCESS FROM NODE 160.00 TO NODE 128.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 129.00 DOWNSTREAM(FEET) = 125.76
 FLOW LENGTH(FEET) = 122.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.0 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.52
 ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 0.45
 PIPE TRAVEL TIME(MIN.) = 0.45 Tc(MIN.) = 7.05
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 128.00 = 550.00 FEET.

FLOW PROCESS FROM NODE 128.00 TO NODE 130.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 125.76 DOWNSTREAM ELEVATION(FEET) = 117.50
 STREET LENGTH(FEET) = 156.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.65
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(Feet) = 0.24
 HALFSTREET FLOOD WIDTH(Feet) = 5.47
 AVERAGE FLOW VELOCITY(Feet/Sec.) = 3.96
 PRODUCT OF DEPTH&VELOCITY(Ft*ft/sec.) = 0.93
 STREET FLOW TRAVEL TIME(Min.) = 0.66 Tc(Min.) = 7.70
 100 YEAR RAINFALL INTENSITY(Inch/Hour) = 4.984
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100
 S.C.S. CURVE NUMBER (AMC II) = 0
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.727
 SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 2.42
 TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 2.83

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(Feet) = 0.27 HALFSTREET FLOOD WIDTH(Feet) = 7.25
 FLOW VELOCITY(Feet/Sec.) = 4.39 DEPTH*VELOCITY(Ft*ft/sec.) = 1.19
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 130.00 = 706.00 FEET.

FLOW PROCESS FROM NODE 130.00 TO NODE 127.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 108.06 DOWNSTREAM(Feet) = 107.84
 FLOW LENGTH(Feet) = 4.50 MANNING'S N = 0.013
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.1 INCHES
 PIPE-FLOW VELOCITY(Feet/Sec.) = 8.94
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 2.83
 PIPE TRAVEL TIME(Min.) = 0.01 Tc(Min.) = 7.71
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 127.00 = 710.50 FEET.

FLOW PROCESS FROM NODE 127.00 TO NODE 127.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(Min.) = 7.71
 RAINFALL INTENSITY(Inch/Hr) = 4.98
 TOTAL STREAM AREA(ACRES) = 0.78
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.83

FLOW PROCESS FROM NODE 103.00 TO NODE 136.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 150.62

DOWNSTREAM ELEVATION(FEET) = 145.21

ELEVATION DIFFERENCE(FEET) = 5.41

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.849

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.27

TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.27

FLOW PROCESS FROM NODE 136.00 TO NODE 137.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====

UPSTREAM ELEVATION(FEET) = 145.21 DOWNSTREAM ELEVATION(FEET) = 117.57

STREET LENGTH(FEET) = 543.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.25

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.22

HALFSTREET FLOOD WIDTH(FEET) = 4.65

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.73

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.82

STREET FLOW TRAVEL TIME(MIN.) = 2.43 Tc(MIN.) = 5.28

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.361

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.810

SUBAREA AREA(ACRES) = 0.38 SUBAREA RUNOFF(CFS) = 1.96

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 2.22

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.44

FLOW VELOCITY(FEET/SEC.) = 4.16 DEPTH*VELOCITY(FT*FT/SEC.) = 1.06

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 137.00 = 638.00 FEET.

FLOW PROCESS FROM NODE 137.00 TO NODE 127.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 108.72 DOWNSTREAM(FEET) = 107.84

FLOW LENGTH(FEET) = 18.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 8.51

ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 2.22

PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 5.31

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 127.00 = 656.00 FEET.

FLOW PROCESS FROM NODE 127.00 TO NODE 127.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:

TIME OF CONCENTRATION(MIN.) = 5.31

RAINFALL INTENSITY(INCH/HR) = 6.33

TOTAL STREAM AREA(ACRES) = 0.43

PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.22

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	21.17	5.07	6.526	3.97
2	2.83	7.71	4.980	0.78
3	2.22	5.31	6.334	0.43

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	25.15	5.07	6.526
2	24.71	5.31	6.334
3	20.73	7.71	4.980

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 25.15 Tc(MIN.) = 5.07

TOTAL AREA(ACRES) = 5.2

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 127.00 = 990.00 FEET.

FLOW PROCESS FROM NODE 127.00 TO NODE 140.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 107.84 DOWNSTREAM(FEET) = 106.00

FLOW LENGTH(FEET) = 46.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 14.31

ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 25.15

PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 5.13

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 140.00 = 1036.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

FLOW PROCESS FROM NODE 130.00 TO NODE 141.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 40.00

UPSTREAM ELEVATION(FEET) = 117.50

DOWNSTREAM ELEVATION(FEET) = 114.93

ELEVATION DIFFERENCE(FEET) = 2.57

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.776

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.16

TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.16

FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<

UPSTREAM ELEVATION(FEET) = 114.93 DOWNSTREAM ELEVATION(FEET) = 110.22
STREET LENGTH(FEET) = 126.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.45
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.16
HALFSTREET FLOOD WIDTH(FEET) = 1.50
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.65
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.57
STREET FLOW TRAVEL TIME(MIN.) = 0.58 Tc(MIN.) = 2.35
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.59
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.75

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.20 HALFSTREET FLOOD WIDTH(FEET) = 3.54
FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.60
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 142.00 = 166.00 FEET.

FLOW PROCESS FROM NODE 142.00 TO NODE 142.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 2.35
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.14
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.75

FLOW PROCESS FROM NODE 144.00 TO NODE 142.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00
UPSTREAM ELEVATION(FEET) = 115.00
DOWNSTREAM ELEVATION(FEET) = 110.22
ELEVATION DIFFERENCE(FEET) = 4.78
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.160
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.454
SUBAREA RUNOFF(CFS) = 0.17
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.17

*****
FLOW PROCESS FROM NODE 142.00 TO NODE 142.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.16
RAINFALL INTENSITY(INCH/HR) = 6.45
TOTAL STREAM AREA(ACRES) = 0.06
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
    1         0.75      2.35      6.587         0.14
    2         0.17      5.16      6.454         0.06

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
    1         0.83      2.35      6.587
    2         0.91      5.16      6.454

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 0.91 Tc(MIN.) = 5.16
TOTAL AREA(ACRES) = 0.2
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 142.00 = 166.00 FEET.

*****
FLOW PROCESS FROM NODE 142.00 TO NODE 139.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

```

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 106.70 DOWNSTREAM(FEET) = 106.40
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.04
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.91
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 5.26
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 139.00 = 191.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 139.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.26
RAINFALL INTENSITY(INCH/HR) = 6.37
TOTAL STREAM AREA(ACRES) = 0.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.91

FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 117.57
DOWNSTREAM ELEVATION(FEET) = 114.93
ELEVATION DIFFERENCE(FEET) = 2.64
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.136
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.27

FLOW PROCESS FROM NODE 138.00 TO NODE 139.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 114.93 DOWNSTREAM ELEVATION(FEET) = 110.22
STREET LENGTH(FEET) = 91.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.40
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FT) = 0.16
HALFSTREET FLOOD WIDTH(FT) = 1.50
AVERAGE FLOW VELOCITY(FT/SEC.) = 4.29
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.67
STREET FLOW TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 3.49
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810
SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.53

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FT) = 0.16 HALFSTREET FLOOD WIDTH(FT) = 1.50
FLOW VELOCITY(FT/SEC.) = 4.29 DEPTH*VELOCITY(FT*FT/SEC.) = 0.67
LONGEST FLOWPATH FROM NODE 137.00 TO NODE 139.00 = 171.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 139.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.49
RAINFALL INTENSITY(INCH/HR) = 6.59
TOTAL STREAM AREA(ACRES) = 0.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.53

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.91	5.26	6.372	0.20
2	0.53	3.49	6.587	0.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.41	3.49	6.587
2	1.42	5.26	6.372

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 1.42 Tc(MIN.) = 5.26
TOTAL AREA(ACRES) = 0.3
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 139.00 = 191.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 140.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 106.40 DOWNSTREAM(FEET) = 106.00
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.11
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.42
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.43
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 140.00 = 231.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 11

>>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.42	5.43	6.249	0.30

LONGEST FLOWPATH FROM NODE 130.00 TO NODE 140.00 = 231.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	25.15	5.13	6.482	5.18

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 140.00 = 1036.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
------------------	-----------------	--------------	--------------------------

1	26.49	5.13	6.482
2	25.66	5.43	6.249

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.49 Tc(MIN.) = 5.13
 TOTAL AREA(ACRES) = 5.5

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

FLOW PROCESS FROM NODE 146.00 TO NODE 147.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 116.27

DOWNSTREAM ELEVATION(FEET) = 110.79

ELEVATION DIFFERENCE(FEET) = 5.48

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.837

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.587

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.69

TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.69

FLOW PROCESS FROM NODE 147.00 TO NODE 140.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 107.79 DOWNSTREAM(FEET) = 106.00

FLOW LENGTH(FEET) = 3.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 15.91

ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.69

PIPE TRAVEL TIME(MIN.) = 0.00 Tc(MIN.) = 2.84

LONGEST FLOWPATH FROM NODE 146.00 TO NODE 140.00 = 98.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<
=====

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.69	2.84	6.587	0.13

LONGEST FLOWPATH FROM NODE 146.00 TO NODE 140.00 = 98.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	26.49	5.13	6.482	5.48

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 140.00 = 1036.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	15.37	2.84	6.587
2	27.17	5.13	6.482

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 27.17 Tc(MIN.) = 5.13
TOTAL AREA(ACRES) = 5.6

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.482
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7951
SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 1.00
TOTAL AREA(ACRES) = 5.8 TOTAL RUNOFF(CFS) = 29.89
TC(MIN.) = 5.13

FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<
=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 124.30 RAIN INTENSITY(INCH/HOUR) = 0.83
TOTAL AREA(ACRES) = 5.80 TOTAL RUNOFF(CFS) = 0.12

FLOW PROCESS FROM NODE 140.00 TO NODE 300.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) =	94.20	DOWNSTREAM(Feet) =	92.00
FLOW LENGTH(Feet) =	110.00	MANNING'S N =	0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO	6.000		
DEPTH OF FLOW IN 6.0 INCH PIPE IS	1.6 INCHES		
PIPE-FLOW VELOCITY(Feet/Sec.) =	2.78		
ESTIMATED PIPE DIAMETER(INCH) =	6.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	0.12		
PIPE TRAVEL TIME(Min.) =	0.66	Tc(Min.) =	124.96
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 300.00 =	1146.00 FEET.		

+-----+
| ENTER HYDROCAD OUTPUT REPORT AT THE FOLLOWING NODE 140 TO 140 |
| |
+-----+

FLOW PROCESS FROM NODE 300.00 TO NODE 700.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) =	92.00	DOWNSTREAM(Feet) =	84.00
FLOW LENGTH(Feet) =	25.00	MANNING'S N =	0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO	6.000		
DEPTH OF FLOW IN 6.0 INCH PIPE IS	0.8 INCHES		
PIPE-FLOW VELOCITY(Feet/Sec.) =	7.59		
ESTIMATED PIPE DIAMETER(INCH) =	6.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	0.12		
PIPE TRAVEL TIME(Min.) =	0.05	Tc(Min.) =	125.01
LONGEST FLOWPATH FROM NODE 103.00 TO NODE 700.00 =	1171.00 FEET.		

+-----+
| END FLOWS TO POC-A |
| |
+-----+

=====

END OF STUDY SUMMARY:

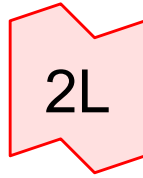
TOTAL AREA(ACRES)	=	5.8	TC(Min.) =	125.01
PEAK FLOW RATE(CFS)	=	0.12		

=====
=====
END OF RATIONAL METHOD ANALYSIS

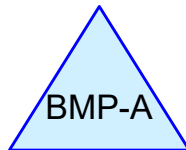


APPENDIX D

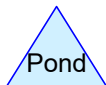
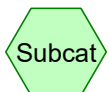
Hydrograph and Detention Calculations



BMP-A 100-YR
INFLOW



BMP-A



Routing Diagram for 3733 - HydroCAD (22-0908)

Prepared by {enter your company name here}, Printed 9/8/2022
HydroCAD® 10.00-24 s/n 10097 © 2018 HydroCAD Software Solutions LLC

Summary for Pond BMP-A: BMP-A

Inflow = 29.89 cfs @ 4.08 hrs, Volume= 0.974 af
 Outflow = 0.12 cfs @ 6.07 hrs, Volume= 0.655 af, Atten= 100%, Lag= 119.3 min
 Primary = 0.12 cfs @ 6.07 hrs, Volume= 0.655 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs
 Peak Elev= 106.71' @ 6.07 hrs Surf.Area= 5,600 sf Storage= 41,051 cf

Plug-Flow detention time= 2,479.3 min calculated for 0.655 af (67% of inflow)
 Center-of-Mass det. time= 2,448.3 min (2,660.7 - 212.4)

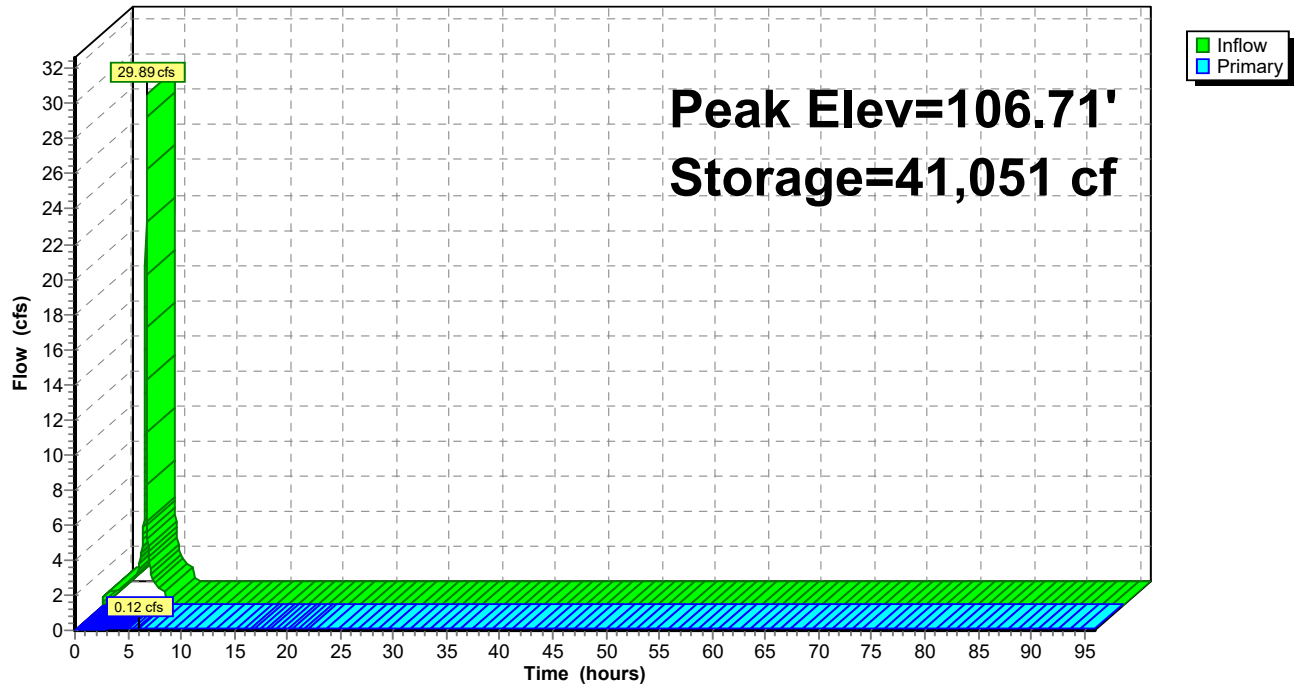
Volume	Invert	Avail.Storage	Storage Description
#1	97.25'	51,100 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
97.25	5,600	0.0	0	0	5,600
103.75	5,600	95.0	34,580	34,580	7,324
106.00	5,600	20.0	2,520	37,100	7,921
108.50	5,600	100.0	14,000	51,100	8,584

Device	Routing	Invert	Outlet Devices
#1	Primary	97.25'	24.0" Round Culvert L= 25.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 97.25' / 84.00' S= 0.5300 '/' Cc= 0.900 n= 0.013, Flow Area= 3.14 sf
#2	Device 1	97.25'	1.2" Vert. Orifice C= 0.600
#3	Device 1	107.50'	36.0" x 36.0" Horiz. Grate C= 0.600 in 36.0" x 36.0" Grate (100% open area) Limited to weir flow at low heads
#4	Device 1	107.50'	36.0" x 36.0" Horiz. Grate C= 0.600 in 36.0" x 36.0" Grate (100% open area) Limited to weir flow at low heads
#5	Device 2	97.25'	5.000 in/hr Exfiltration over Surface area below 106.00'

Primary OutFlow Max=0.12 cfs @ 6.07 hrs HW=106.71' (Free Discharge)

1=Culvert (Passes 0.12 cfs of 54.98 cfs potential flow)
 2=Orifice (Orifice Controls 0.12 cfs @ 14.77 fps)
 5=Exfiltration (Passes 0.12 cfs of 0.65 cfs potential flow)
 3=Grate (Controls 0.00 cfs)
 4=Grate (Controls 0.00 cfs)

Pond BMP-A: BMP-A**Hydrograph**

Grate Capacity Calculator

Using Sharp Crested Weir Formula equation (5-10) $Q = CLH^{1.5}$ where Coefficient C is 3.3 (Brater and King)

Weir Coefficient

3.3

GRATE INLET CAPACITY				
INLET TYPE	PERIMETER (FT)	HEAD (FT)	GRATE/CLOG FACTOR	Q _{CAP} (CFS)
3' Catch Basin (BMP-A)	12	1.0	2	19.800
3' Catch Basin (BMP-A)	12	1.0	2	19.800
TOTAL CAPACITY =				39.600

VOLUME AREA CALCULATION - POC-A					
EXISTING			PROPOSED		
P ₆ =	0.208	(FT)	P ₆ =	0.208	(FT)
C =	0.45		C =	0.81	
A =	108,029	(FT ²)	A =	252,567	(FT ²)
VOL =	10,128	(FT ³)	VOL =	42,621	(FT ³)
Δ =			32,493 (FT ³)		

VOLUME AREA CALCULATION - POC-B					
EXISTING			PROPOSED		
P ₆ =	0.208	(FT)	P ₆ =	0.208	(FT)
C =	0.45		C =	0.45	
A =	256,568	(FT ²)	A =	111,949	(FT ²)
VOL =	24,053	(FT ³)	VOL =	10,495	(FT ³)
Δ =			(13,558) (FT ³)		

BASIN-A STORAGE CAPACITY			
MEDIA	SURFACE AREA (S _A) (FT ²)	DEPTH OF MEDIA (D) (FT)	VOID RATIO (VR)
RTANK	5,600	6.5	0.95
SOIL MEDIA	5,600	1.5	0.2
PONDING	5,600	1.5	1.0
TOTAL BASIN VOL =	44,660	(FT ³)	

BASIN SUMMARY		
REQUIRED STORAGE VOLUME =	32,493	(FT ³)
TOTAL PROVIDED BASIN VOLUME =	44,660	(FT ³)
MEETS VOLUME REQUIREMENTS?	YES	